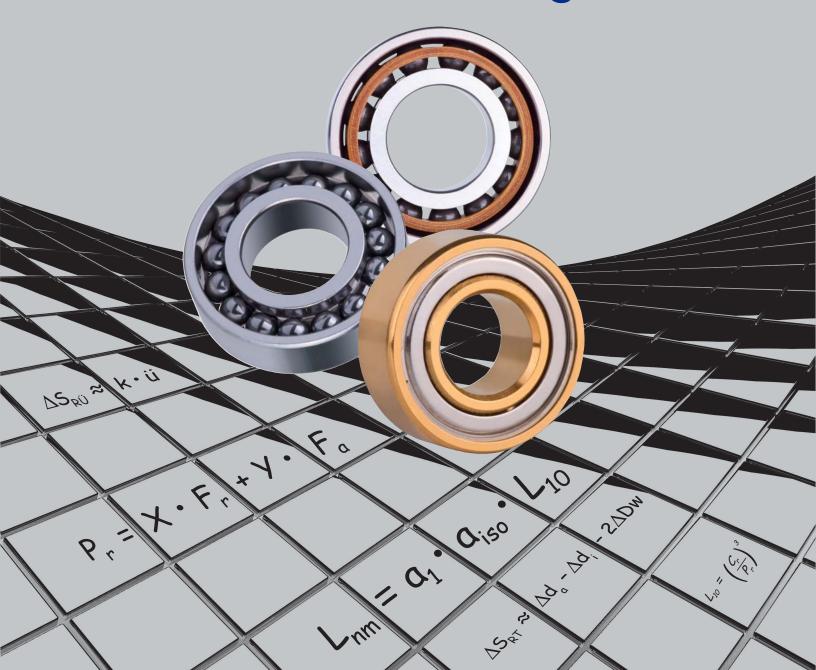


High-Precision Ball Bearings Product Catalog



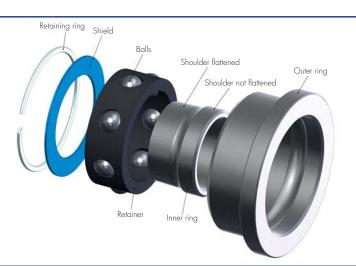


Designation system of radial ball bearings – metric / inch



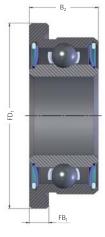
								Closure			
	-			LE	625	5		-	P		C
	HY		SS	F	3/1	6		-Z	ABEC		К
	ZO		SV	E	625/60	3938		-2Z			D
			S					-RZ			
			SA					-RS			
			N					-VZ			
			NZ					-VS			
								-TS			
-	Steel balls	-	100Cr6	LE Bearing unit	625	Metric	-	Open ball bearings	Standard tolerance grade	Metric of bearing	deep groove radial as
		SS	X65Cr13	F Flange	3/16	Inch	-Z	Single shield	PO		
HY	Ceramic balls made from	sv	X30CrMoN15-1	E Extended	625/XXXXXX		-2Z	Double shield	or ABEC1 not marked	- C2 C3	Standard clearance Narrower than standard Slightly increased radial
		S	440C	inner ring		drawing	-RZ	Single Perbunan rubber shield,	P tolerance grade for metric	C4	clearance Increased radial clearance
zo	Ceramic balls	SA	Antimagnetic material					non-contact	bearings in P6 , P5 , P4 and P2	C5	Strongly increased radial clearance
	made from ZrO ₂		nbination balls Full ceramic				-RS	Single Perbunan rubber contact seal	ABEC tolerance grade		ict values depend on the
		IN	bearings (balls, IR, AR)				-vz	Single Viton shield, non-contact	for inch bearings in ABEC3 ,		dimensions, see capter assification of radial ce".
			of silicon nitride				-vs	Single Viton	ABEC5 etc.		radial clearance: f.e.
		NZ	Full ceramic bearings (balls, IR, AR)				-TS	contact seal Single Teflon®	Special tolerance grades: ABEC9P ,	C1/5 C4/8	1 to 5 μm 4 to 8 μm 5 10 to 15 μm
			made from zirconium oxide				15	contact seal	P4A, P4S,		14 to 20 μm
										Defined K02 K13 K46 K58 D	ep groove radial bearings radial clearance: f.e. 0 to .0002" .0001" to .0003" .0004" to .0006" .0005" to .0008" Followed a by number indicates contract angle ball bearings Contact angle 15°
			ner materials ilable on request							E	Contact angle 25°

Designation system of radial ball bearings – metric / inch



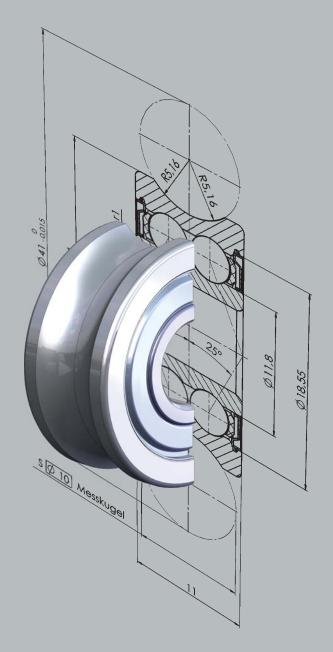
	GPR GPA R()		X XB XD X4 X4B X4D		-1 -2 -3 -4		/ L M S		E J J1 TXHB TXA 		– % MG	G L L299 B
GPR GPA R()	Noise test (standard 100%) Axial vibration test Followed by a number indicates starting torque with standard load, max. 16 µNm	X XB XD X4 X4B X4D	Bore and outside diameter graded in 2 classes Bore graded in 2 classes Outside diameter graded in 2 classes Bore and outside diameter graded in 4 classes Bore graded in 4 classes Outside diameter graded in 4 classes	-2	Back to back (O-arrangement) Face to face (X-arrangement) Tandem Universally paired Universally paired Exam Deep groove ro -1/5 (= O-arra 5 N pro	spin bea L M S Prelo than poss ple: dial ingen	value in [N] bad for dle ball rings light medium strong bad other L, M, S sible bearings: nent with	E J J1 TXHB Examp T19HB For infa and ott see cha	proove radial bearings 2-pc. steel retainer 2-pc. stainl. steel retainer 2-pc. stainl. steel hybrid retainer Machined one-piece snap retainer, X stands for a number and defines the material le: Machined synthetic snap retainer made from XTRAIon ormation about TXA her retainer variants apter "Retainers for ire ball bearings"	%	No data Standard quantity In % of the free space only for lubricated bearings) Lubricant quantities spe- cified in mg or indication of quantity range e.g. 10–15% or 6–10/MG	 Grease Oil dry bearing Special treatment
				Spir UM	mple: ndle ball bearings: . (= universally mat dium preload)		pairs,	VAC1 VAC2 VF Spindl AC1 AC2 Examp AC1TA ground retaine	mplement ball bearing Full complement variations be ball bearings Outer ring shoulder ground Inner ring shoulder ground le: Outer ring shoulder led & machined solid r made from fabric- zed phenolic resin			











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Our Company

As a global corporation with more than 500 employees, GRW is headquartered in Rimpar, near Würzburg, with assembly facilities in Prachatice (Czech Republic) and a direct sales office in the USA

GRW is the premier developer and manufacturer of miniature precision ball bearings, assemblies and accessory parts utilizing state-of-the-art equipment and manufacturing processes. We specialize in production of high precision, small, miniature and instrument bearings as well as spindle bearings and bearing units. GRW also welcomes the opportunity to design, develop and produce customized applications using customer specifications.

Our radial ball bearings range in bores from 1 mm to 35 mm with outer diameters from 3 mm to 47 mm meeting any condition from mini series to high volume standard applications.

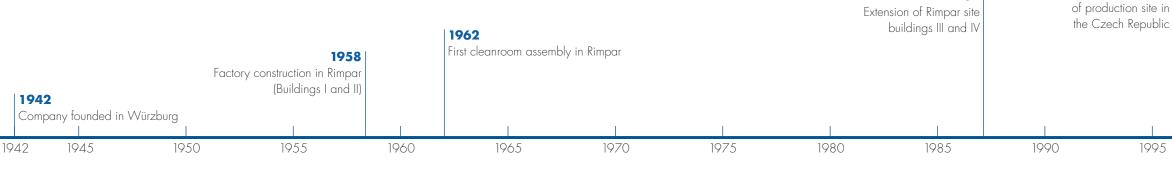
GRW bearings are produced in both metric and inch dimensions making them truly applicable to any customer in the world. Whether your application reguires mini series, standard high volume or customized specifications, you can always rely upon GRW to meet any requirement or challenge.

GRW complies with the highly recognized standard of quality in process and performance as evident by our ISO certification, DIN EN ISO 9001:2008.



Headquarter and production site at Rimpar

GRW... the premier provider for customized high-precision ball bearing solutions.



Preface

"Miniature precision meets extreme demands"

In order to successfully meet the challenges of the market, our products are being continuously developed and their performance improved, based on the latest innovations from GRW.

Developments that we have achieved in the areas of product design, ball bearing steels, retainer design and materials, lubricants and surface coatings, are the basis for the technological leadership the company has today.

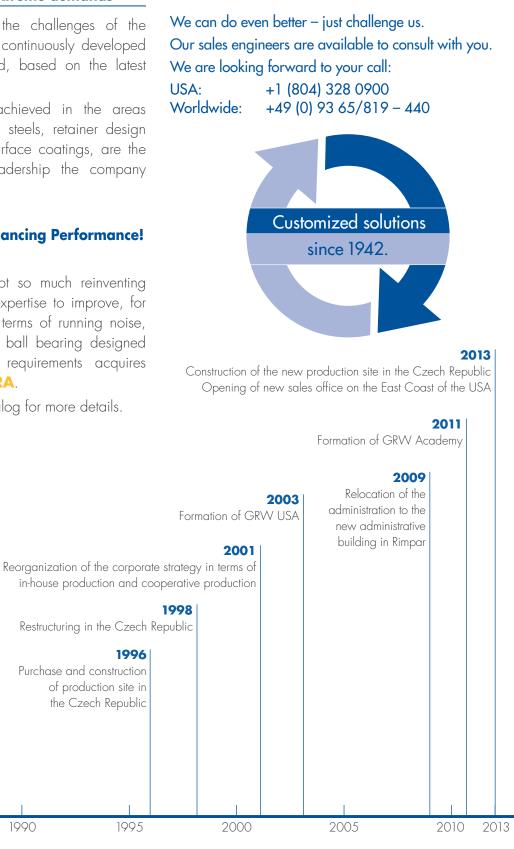
Our latest advance: XTRA – Enhancing Performance!

With GRW XTRA, we are not so much reinventing the ball bearing but using our expertise to improve, for example, performance levels in terms of running noise, service lifetime and speed! The ball bearing designed by GRW to your individual requirements acquires superior performance due to XTRA.

See page 79 of this product catalog for more details.

1987







Materials for rings and balls

GRW ball bearings are manufactured by using technological advancements in steel production and heat treatment. Our ball bearings are made of chrome steel (100Cr6), stainless steel (X65Cr13), or high corrosionresistant steel (X30CrMoN 15-1). It is now possible to achieve comparable load ratings for all these steel types.

Ceramic balls, e.g. hybrid ball bearings, can be used in all versions as required by your application.



Materials for rings and balls

Hybrid ball bearings

GRW hybrid, or ceramic ball bearings are made of one of the steels previously mentioned as well as silicon nitride (Si_3N_4) or zirconium oxide (ZrO_2) , both which offer specific benefits.

These types of bearings are used most commonly in dental handpieces, spindle bearings and vacuum pumps to extend speed limits or increase bearing stiffness.

Using GRW Si₂N₄ ceramic balls reduces load rating by 30 %, while the dynamic load rating remains unaffected.

The low affinity to other materials allows a particularly low adhesive wear. As a result, hybrid or ceramic bearings provide extended lifetime run times when used in mixedtorque applications.

Prefix	Unit	-	55	sv	НҮ	ZO
DIN		100Cr6	X65Cr13	X30CrMoN 15-1	Si ₃ N ₄	ZrO ₂
DIN		1.3505	1.4037	1.4108		
SAE		52100				
Properties						
Density	[g/cm ³]	7.81	7.7	7.7	3.2	6.0
Hardness	[HRE]	> 60	> 58	> 58	> 75	> 69
E-module	[GPa]	212	220	223	320	200
Expansion coefficient	[x 10 ⁻⁶ °C]	11.0	10.5	10.4	3.0	10.5
Corrosion resistance	[-]	limited	good	very good	very good	good
Electrical conductivity	[-]	conductor	conductor	conductor	insulator	insulator
Magnetism	[-]	magnetic	magnetic	magnetic	non magnetic ⁽¹⁾	non magnetic

⁽¹⁾ May contain magnetic parts for production technology reasons

Our sales engineers will gladly inform you about the chemical resistance properties of the materials. Subject to change.

Closures

Integrated ball bearing shields and seals provide two vital purposes: to prevent dirt and foreign particles from infiltration and to prevent lubricants from leaking out.

Non-contact shields

Together with the shoulder of the inner ring, the closure creates a narrow gap. Similar to open ball bearings, this closure neither increases running friction nor limits the maximum permissible speed because the shields do not touch the inner ring. This is sufficient for most applications. Shields prevent contamination with dirt particles but cannot achieve a hermetic seal

Metal shields Z

For the majority of our bearings, shields are stamped from corrosion-resistant steel. They are fastened and secured to the outer ring by means of a circlip and can thus be removed. Bearings can also be fitted with pressed-in shields made from a deep drawn steel sheet; these shields cannot be removed

RZ/VZ rubber seal

The RZ closure is made of synthetic buna N rubber with a steel support shield and can be used at temperatures from -30 $^{\circ}$ C to +120 $^{\circ}$ C.

The VZ closure is made of synthetic Viton fluoroelastomer with steel support shield and can be used at temperatures from -20 °C to +230 °C.

Both shield types are secured by snap fit.

Contact seals

This type of seal touches the shoulder of the inner ring, causing an increase in start up and running torque.

Teflon[®] seals can be used at working temperatures of -240 °C to +300 °C. The friction is lower than for rubber seals due to the low friction combination (PTFE / steel) and the low contact force of the sealing lip.



Teflon[®] seal TS

sheet that is fastened in the outer ring by means of a circlip. TS seals are universally resistant to chemicals. Bearings using TS seals are normally made of corrosion-resistant steel. In appropriately large quantities, TS seals can also be made available for chrome steel bearings. RS/VS seals The RS seal is made of synthetic buna N rubber with a steel support shield and can be used at temperatures from -30 $^{\circ}$ C to +120 $^{\circ}$ C. The VS seal is made of synthetic Viton fluoroelastomer with a steel support shield and can be used at temperatures from -20 °C to +230 °C. Both shield types are secured by snap fit. **Custom shields and seals** GRW can also manufacture custom accessories and combinations of different shields and seals to meet your specifications.

The TS seal is made of a glass-fiber reinforced Teflon®

- For improved sealing effect between steel shields and outer ring GRW offers a special laminated shield.
- In this context, we would like to point out that certain lubricants cannot be used with all closures. Please consult our sales engineers about difficult applications.





Retainers for miniature ball bearings

Retainers are vital for efficient operation of ball bearings. First, they keep the balls separated and evenly spaced, ensuring a uniform distribution of load and thereby reducing heat while enhancing the bearing life expectancy.

Secondly, the retainer guides the balls in the loadfree zone and prevents the balls from dropping out of separable bearings. Using our customized designs and materials, retainers can be manufactured to meet any application. We recommend usage of a two-part ribbon retainer for the majority of applications.

In this context, we would like to point out that certain lubricants cannot be used with all retainers.

GRW retainer designation	Illustration	Description/ material	Scope of application / purpose
E J		Two-piece retainer made from – steel sheet (E) – stainless steel sheet (J) Retainer clamping types: – without additional sign = standard – F = retainer tightly clamped – L = retainer loosely clamped	E/J: Standard retainer for deep groove radial bearings. For stainless bearings: retainer always made from stainless steel sheet. To avoid torque peaks as far as possible, this retainer can also be mounted in a loosely clamped condition. JH: For deep groove radial bearings.
JH		One-piece snap-type retainer made of stainless steel (JH)	Used primarily for small ball bearings and low to medium speeds.
J1 XTRAflow	\bigcirc	Two-piece hybrid material retainer made from — stainless steel sheet (J1)	For applications which require minimal friction and long life even at poor lubrication conditions.
TNH	0	One-piece molded synthetic snap retainer.	For deep groove radial bearings in medium speed range with good running and torque characteristics. Working temperature from -30°C to +80 °C, short term up to +100 °C.
TNXH	O	One-piece molded synthetic snap retainer made from glass fiber reinforced plastic. X stands for a number and defines the material.	For deep groove radial bearings in a speed range above that of the TNH retainer. Working temperature from -30°C to +120 °C, short term up to +180 °C.
THA THB		Machined one-piece snap retainer made from fiber-reinforced phenolic resin. A = outer ring guided B = inner ring guided	For deep groove radial bearings with very high speeds. High rigidity and emergency running properties. Working temperature from -50°C to +130°C. Can be impregnated with oil.
TXHA TXHB XTRAIon		Machined one-piece snap retainer made from a special material. X stands for a number and defines the material. A = outer ring guided B = inner ring guided	For deep groove radial bearing with very high speeds. High rigidity and emergency running properties. Working temperature, depending on the material, up to +250°C or even +300°C.
		These retainer can also be ordered with our service life! Please find more information abc	new retainer material XTRAIon , for even longer but XTRAIon on page 82.



As not every retainer is available for all sizes, please contact us for additional information. We will gladly recommend other bearing and retainer designs as well as retainer materials for special requirements.

developing new options or enhancing existing variations. As a result, GRW is the sole owner of some exclusive licenses and patents for using specifically developed retainer materials such as the new developed premium material **XTRAIon**. Detailed information concerning **XTRAIon** you can find on page 82.

GRW offers some of the highest performance synthetic materials including **Vespel[®]**, **Torlon[®]**, **PEEK**, **PTFE** and Meldin[®] as well as various metallic materials and phenolic resins. In addition to using proven materials, GRW, in close cooperation with its customers and suppliers, is constantly



ion/ material	Scope of application / purpose
parable, parable,	For separable angular contact ball bearings/ spindle bearings with highest speeds. High rigidity. Working temperature from -50 °C to +130 °C. Can be impregnated with oil.
eparable, 1g eparable, ber and defines the	For separable angular contact ball bearings/ spindle bearings with highest speeds. High rigidity and emergency running properties. Working temperature, depending on the material, up to +250 °C or even +300 °C.
	new retainer material XTRAIon , for even longer but XTRAIon on page 82.
ce solid retainer made d phenolic resin. led ed 2 types. Non-separable.	For angular contact bearings/spindle ball bearings with highest speeds. High rigidity and emergency running properties. Working temperature from -50 °C to +130 °C. Can be impregnated with oil.
ce solid retainer made erial. ber and defines the led 2 types. Non-separable.	For angular contact bearings/spindle ball bearings with highest speeds. High rigidity and emergency running properties. Working temperature, depending on the material, up to +250 °C or even +300 °C.
	new retainer material XTRAIon , for even longer but XTRAIon on page 82.
earing, without retainer, nbled. elieved on outer ring elieved on inner ring ring shoulder ground on	Used for medium speeds, high radial loads and high axial loads in one direction.
all bearing, without able, with filling slot for	Used for medium speeds and high radial loads.



Lubricants

Why do bearings need lubricants?

Miniature ball bearings are perfect for high stress environments, but require special lubricants to minimize wear, in order to increase operational life, performance, and safety of the product.

GRW lubricants provide permanent lubrication to minimize sliding friction between balls, rings and retainer. This prevents excessive wear and thermal overheating, protecting balls and raceway from micro-welding and thereby extending operational life while reducing running noise. The bearing application specification determines the best type of lubrication to use.

Grease lubrication

Thanks to their ability to dispense a lubricating film over time, grease lubricants offer an additional advantage when being used in maintenance-free applications.

Most of GRW bearings are grease-lubricated, with approximately 300 different greases to select from. The standard recommended amount of grease (lubricant quantity) is one-third (33%) of the remaining free space in the bearing. Grease quantities deviating from this standard are indicated in the bearing part number just before the type of lubricant, preferably in percent or alternatively in milligrams.

Furthermore, our customers can choose other special treatments for grease applications, for example a



dispersion or a thin defined layer of grease. Here the designation system differentiates between TF (thin film), MF (medium film) and SF (strong film).

Oil lubrication

Miniature bearings lubricated with oil may offer advantages over those lubricated with grease.

Oil is primarily used in applications where a minimal torque is required. In particular, high speed spindle bearings are typically lubricated with high performance oils.

When compared to grease lubrication, oil lubrication sometimes uses a dispersion of oil and a solvent to achieve a better distribution of oil throughout the bearing.

With more than 100 special oils to choose from, GRW can help you to select the oil that perfectly matches your application. If no special lubrication is needed, all of our bearings whether open or shielded, are preserved with light instrument oil when they leave our factory.

Proper lubrication practices

At GRW, all bearings are lubricated during final assembly under clean-room conditions. Since dust particles can cling to the oiled or greased bearings, it is important that the customer maintains a high standard of cleanliness in their application. In addition we recommend using a clean-room for removal of the bearings from their package and during assembly.

With greased bearings, the specified quantity of lubricant, accurate to milligrams, is injected directly into specified locations of the miniature ball bearing. Usually the lubricant is injected from only one side, however it is also possible to lubricate each bearing from both sides for better distribution.

For lubrication with standard oils, the oil is poured over the bearing which is then spun. Alternatively, a specified oil quantity can be directly injected into the bearing.

Solid lubricants

Non-lubricated bearings may be used in certain Sterilization (autoclaving) is mandatory for the proper applications and are also available from GRW. These use and maintenance of medical instruments according non-lubricated bearings are typically required for ultra-high to the guidelines of the Robert-Koch Institute. This applies vacuum (UHV) temperature extremes and for applications to the hygienic treatment of surgical devices and dental in aviation and aerospace. Here the operating conditions turbines that depend on miniature ball bearings. go beyond the functional limits of oil and grease GRW's stainless steel and retainer materials can easily lubricants. The use of a bearing without a protective withstand sterilization in an autoclave subjected to lubricant will negatively impact its tribological system; superheated steam, where most lubricants do not however lubrication with solids is a viable alternative survive. Combined with the extreme high speed stresses of dental turbines, these lubricants are required to provide exceptional surface adhesion and GRW offers its customers a variety of different dry film sterilization resistance.

coatings. Applying thin layers of precious, Wolfratherm® or MoS₂ provides protection and lubrication for the bearina.

For oil or grease lubricated bearings, this process ensures reliable performance in case of lubricant deprivation (emergency running conditions). In GRW's part numbering system, the surface treatment of bearing components is indicated by a "B", followed by a four-digit number code indicating the type of surface treatment.

Custom treatments

In addition to varying lubricants and surface treatments, GRW can custom treat bearing components to improve tribological behavior. For example, the phenolic retainer can be vacuum-impregnated with oil (up to 5% by weight). The benefit of a vacuum-impregnated retainer is its ability to release small amounts of lubricant continually during operation. This process improves the general lubrication performance and ensures emergency running properties in lube deprived situations.



Lubricants in medical applications

As manufactured, GRW bearings utilize a range of lubricants that are resistant to the sterilization process and well suited for dental and surgical devices. This optimization results in a longer life under extreme environmental conditions.

XTRAlube

For enhanced performance and longer life time we recommend the new by GRW developed lubrication XTRAlube.

More information about XTRAlube you can find on page 81.

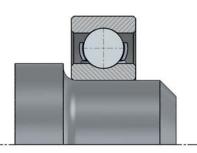


Shaft and housing shoulders

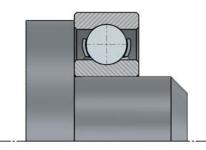
Certain design and assembly factors are critical for optimum performance of bearings. For instance, shaft and housing shoulders should accurately allow axial load to be transferred to the inner and outer ring without permitting the rings to tilt in opposite directions.

The associated dimension tables provide limits for the largest (d_{a max}) and the smallest (d_{a min}) permissible shoulder diameter for the inner ring and the largest permissible shoulder diameter for the outer ring (D_{a max}).

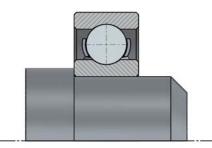
See Dimension Tables on pages 30 to 57.



Wrong, Shaft radius greater r_{s min}



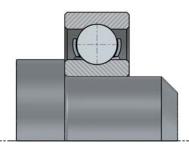
Wrong, Shaft shoulder greater than damax



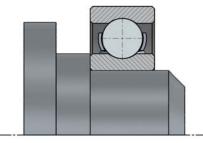
Wrong, Shaft shoulder smaller than d_{a min} Note: Similar examples apply to bearing housings.

Please note the following considerations:

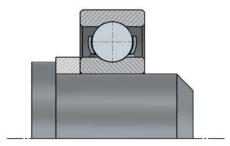
- The housing shoulder diameter for the outer ring must always be smaller than $(D_{a max})$ and the shaft shoulder diameter at the inner ring must not be smaller than (d_{amin}).
- The corner radius between fit and shoulder must not be larger than the corner clearance (r_{emin}) of the bearing. Here an undercut is preferable to a corner radius. The edge radii of the bearing are not designed as a locating surface for the bearing in any way.
- The axial runout of the mating surfaces should not be greater than the maximum axial runout of the bearing used. Otherwise the function of the bearing will be compromised.



Correct, Shaft radius smaller than r_{s min}



Correct, Shaft shoulder equal with inner ring shoulder



Correct, Support ring in place

Special installation configurations

Flanged bearings

Using miniature and instrument bearings with a flange on the outer ring offers several advantages.

Stepped housing bores, which make it impossible or very difficult to maintain accurate alignment of both bearing fits, are no longer necessary. There is also no need for the use of circlips, which create difficulties in small housing bores or thin-walled housings.

Flanged bearings assembled in narrow housings, such as gearboxes, are particularly effective.

With paired bearings, the use of a flanged bearing simplifies the proper assembly and alignment of the bearing. This allows for the accurate axial positioning of the Duplex bearing pair.

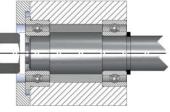
Bearings with extended inner rings

Bearings with an extended inner ring simplify design and mounting of various assemblies. Shims, washers and other spacers are not necessary. Stepped shafts are also redundant.

Bearings with reinforced outer ring

Ball bearings whose outer rings are supported by the proper housing fit can withstand the highest loads. To increase the load capacity of a bearing which is not pressed into a housing, it takes advantage of a reinforced outer ring. These types of bearings can be used as "rollers".

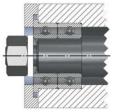




Proper installation, general



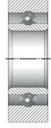
Assembly in narrow housings



Application of a Duplex bearing



Bearings with extended inner ring



Bearings with reinforced outer ring



Fitting tolerances

Among other factors, the fit of the bearing on the shaft and in the housing significantly affects the operational behavior of miniature ball bearings. When selecting fitting tolerances the following criteria should be considered:

Rotation conditions

Rings with circumferential loading should have a tighter fit than rings with a single point load. Circumferential loading occurs when the ring is rotating and the load is static, or when the ring is static and the load is rotating.

Point loading occurs when the rings and loads are both static, or when the rings and loads are both rotating in the same direction with equal speed. Please refer to the table "Shaft tolerances" and "Housing tolerances".

Running accuracy

The same high standards of accuracy and surface quality applicable to the bearings must be applied to the shaft and housing bore.

Loading

Higher loads require a tighter fit between ball bearing, shaft and housing.

Temperature

There may be temperature differences between the bearing and mating components while the bearing is in operation. Dimensional changes caused by differential thermal expansion should be considered when selecting a bearing.

With miniature bearings it is very important to select the proper fit for the highest accuracy and reliability, hence only a close sliding or transition fit is generally required. In addition irregularities on the shaft or in the housing bore are transferred to the relatively thin-walled bearing rings.

In order to improve the fit, it is possible to classify and sort the bore and outside diameters into groups (also refer to the chapter "Calibration of bore and outside diameters"). The values shown in these tables "Shaft tolerances" and "Housing tolerances" are only valid for materials with the same expansion coefficient (11 x 10^{-6} 1/K). For different expansion coefficients, or when there are temperature differences between the bearing rings and the shaft or housing, a tolerance should be selected which ensures the appropriate fit at operating temperature.

Note: For certain environmental conditions, an adhesive may be used to secure the bearing rings. Please contact our sales engineers for additional information.

Recommended fittings

The recommended fits listed below assume mean tolerances obtained from empirical performance data.

Shaft tolerances

Bearing bore Quality →	PO	Р5	Gra	ding	Type of fit
Tolerance in µm Tolerance in .0001 inch →	0/-8 0/-3	0/-5 0/-2	0/-2.5 0/-1	-2.5/-5 -1/-2	
Operating conditions					
Low load Medium speeds No oscillations	-5/-13 -2/-5	-5/-11 -2/-4	-5/-8 -2/-3	-8/-11 -3/-4	Slide fit
Low to medium loads Medium speeds Low oscillations	0/-8 0/-3	0/-6 0/-2.5	0/-3 0/-1.2	-3/-6 -1.2/-2.5	Tight fit
High loads High speeds Oscillations at high frequency	+4/-4 +1.6/-1.6	+4/-2 +1.6/-1	+4/+1 +1.6/+.4	+1/-2 +.4/-1	Press fit

Subject to change.

Housing tolerances

Ball bearing outer diameter Quality → Tolerance in µm	PO 0/-8	P5 0/-5	0/-2.5	ding -2.5/-5	Type of fit
Tolerance in .0001 inch \rightarrow Operating conditions	0/-3	0/-2	0/-1	-1/-2	
Low load Medium speeds No oscillations	+5/-3 +2/-1.2	+5/-1 +2/4	+5/+2 +2/+1	+2/-1 +1/4	Slide fit
Low to medium loads Medium speeds Low oscillations	0/-8 0/-3	0/-6 0/-2.5	0/-3 0/-1.2	-3/-6 -1.2/-2.5	Tight fit
High loads High speeds Oscillations at high frequency	-4/-12 -1.6/-5	-3/-9 -1.2/-3.5	-3/-6 -1.2/-2.5	-6/-9 -2.5/-3.5	Press fit

Subject to change.

Note:

The information on this page applies to steel shafts and housings. For more information on grading, refer to the chapter "Calibration of If applicable, linear expansion coefficients of other materials (e.g. bore and outside diameters". aluminum housings) must be taken into consideration for other operating temperatures.





Load ratings and L-10 life

The static radial load rating Cor

The basic static radial load rating (C_{α}) applies to bearings which rotate at very slow speeds, which are subjected to slow oscillations or are stationary under load. Per DIN ISO 76, the basic static radial load rating is the static radial load corresponding to a calculated contact stress of 4200 N/ mm² at the center of the contact ellipse of the most heavily loaded ball or raceway. If the contact pressure exceeds this maximum permissible value, plastic deformation will occur affecting the efficient operation and the life of the bearing. In other words, the basic static radial load rating is the maximum allowable radial load for the bearing. The basic static radial load rating for hybrid bearings with Si_3N_4 balls will be approximately 30 % lower than for steel ball bearings.

Static bearing capacity

Static loads including radial and axial components must be converted into the static equivalent radial load (P,) to assess the static bearing load capacity. (P,) is the static radial load which causes the same contact stress at the center of the contact ellipse of the most heavily loaded ball or raceway which occurs under actual load conditions. It is defined as follows:

$P_r = X \cdot F_r + Y \cdot F_r$

```
P. : Static equivalent radial load [N]
```

- X : 0.6
- Y : 0.5
- : Largest radial load occurring [N]
- F_a: Largest axial load occurring [N]

Where: $P_r = F_r$ if $P_r < F_r$

Basic dynamic radial load rating C_r

According to DIN ISO 281, the basic dynamic load rating (C) for radial ball bearings is the constant radial load at which a sufficiently large group of apparently identical bearings can endure one million revolutions before showing evidence of material fatigue.

Fatigue load limit C.

The fatigue load limit (C_) is defined as the radial load under which no material fatigue will occur. For ball

bearings manufactured with commonly used high-quality materials, the fatigue load limit is reached at a contact stress of approximately 1500 N/mm².

The load ratings calculated in this Product Catalog have been computed using a curvature of 52-53 % according to DIN ISO 281. Depending on the bearing geometries, the actual load ratings may differ.

Nominal life L₁₀

The "nominal life" (L_{10}) of a group of apparently identical ball bearings is the life in millions of revolutions, or number of hours, that 90 percent of the group will complete or exceed before the first evidence of material fatigue occurs. For a single bearing, (L_{10}) also refers to the life associated with 90 percent reliability.

This calculation per ISO DIN 281 assumes identical operating conditions including a constant lubricating film separating the ball complement from the raceway during the entire life of the bearing.

The L-10 life of miniature ball bearings is calculated as follows:



L₁₀ : basic rating life for a reliability of 90 % [10⁶ revolutions]

C_r : basic dynamic radial load rating [N]

P. : dynamic equivalent radial load fatigue occurs.

Taking a constant speed for granted, then the number of revolutions may also be expressed as L-10 life in hours (L_{10h}) :



with

- L_{10b}: basic rating life L10 [h]
- n : speed of the inner ring $[min^{-1}]$
- C. : basic dynamic radial load rating [N]

P. : dynamic equivalent radial load [N]

Extended modified rating life L_{nm}

In addition to the nominal life rating (L_{10}) , DIN ISO 281 introduced an extended modified life rating (L_m), and adds a life coefficient (a_1) and operating conditions (a_{1SO}) . In application, life rating may be considerably higher or lower than the nominal L-10 life (L_{10}) . The following correlation applies:

$a_{nm} = a_1 \cdot a_{ISO} \cdot L_{10}$

- L_{am} : extended modified rating life [10⁶ revolutions]
- a₁ : Rating life coefficient for a requisite reliability deviating from 90 %
- a_{ire}: Rating life coefficient for consideration of operating conditions
- L₁₀ : basic rating life for a reliability of 90 % [10⁶ revolutions]

Relability a1 acc DIN ISO 281						
Reliability %	L _{nm}	a ₁				
90	L _{1Om}]				
95	L _{5m}	0.64				
96	L _{4m}	0.55				
98	L _{3m}	0.47				
98	L _{2m}	0.37				
99	Llm	0.25				
99.2	L _{O,8m}	0.22				
99.4	L _{O,6m}	0.19				
99.6	L _{O,4m}	0.16				
99.8	L _{O,2m}	0.12				
99.9	L _{0,1m}	0.093				
99.92	L _{0,08m}	0.087				
99.94	L _{0,06m}	0.080				
99.95	L _{0,05m}	0.077				

Rating life coefficient for Relability a, acc DIN ISO 281



The standardized calculation method for the life rating coefficient (a_{1SO}) takes the following factors into account:

- load on the bearing
- lubrication condition
- fatigue limit of the material
- geometry of the bearing
- internal stress of the bearing
- environmental conditions

Significance of the life rating for miniature ball bearings

All standardized methods for calculating the L-10 life assume that failure is attributable to material fatigue. However, this type of failure occurs very rarely in miniature ball bearings. Rather, miniature ball bearing malfunctions are usually attributed to contamination, retainer wear or lubricant failure. Therefore, L-10 life is theoretical and merely a guide. When estimating the L-10 life of a miniature ball bearing, the exact environmental conditions of the application should be considered.



Limiting speeds

Various mechanical and kinematic factors impact the maximum operational speed of a bearing. The following factors can have an effect on the limiting speed:

- Retainer load
- Noise
- Rolling kinematics
- Lubrication
- Heat generated by friction and the environment
- Inner ring slippage and radial play reduction

Retainer loading

In miniature bearings, the speed limit can be determined among other factors by the retainer material and its design.

Practical experience has shown that machined synthetic retainers are better qualified for the highest speeds. These retainers generate smaller imbalance at high speed because of their small mass and the accuracy by which they are manufactured. They are characterized by higher density and elasticity enabling them to withstand the alternating forces generated from ball acceleration and deceleration.

With more than 40 different retainer materials, our product range offers an appropriate technical solution for nearly every application.

Heat

All bearing assemblies have a maximum operating temperature, which ultimately limits the bearing speed. This maximum temperature is not only defined by the bearing's mechanical components, but also by the temperature range of the lubricant. In general, the operating temperature achieved at a certain speed depends on the torque generated in the bearing and the assembly's ability to transfer heat to the environment.

This assumption is the basis for calculating the thermal reference speed as noted in DIN ISO 15312.

Thermal reference speed

The thermal reference speed (n_{o}) defines the speed of the inner ring at which a balance is achieved between the heat generated in the bearing by torgue and the heat flow dissipated through the shaft and housing.

For the standardized calculation method noted in DIN ISO 15312, the following conditions apply:

- Mean ambient temperature $\vartheta_{A_{c}} = +20 \ ^{\circ}\text{C}$
- Static temperature at the outer ring $\vartheta_{1} = +70 \text{ °C}$
- Standard bearings without seals
- 5 % of the static load rating as pure radial load
- Lubricant: mineral oil with a kinematic viscosity of $v = 12 \text{ mm}^2/\text{s}$ at $\vartheta_1 = +70 \text{ °C}$

Significance of the thermal reference speed

The calculation of the thermal reference speed is general and does not take into consideration application specific conditions. As such the thermal reference speed is to be used merely as a guideline value allowing for direct comparison of the different bearing sizes.

Significantly higher speeds can be achieved with special modifications of the components surrounding the bearing and of the bearing itself. Through the use of Si_2N_4 (ceramic) balls, a highly accurate synthetic retainer, a higher bearing tolerance grade and a high-performance lubricant, significantly higher speeds can be achieved.

Elastic behavior of deep groove radial bearings

With ball bearings, two types of deformation have to be The following formula provides an estimation of the distinguished: axial and radial elastic deformation. axial preload:

Axial elastic deformation

The axial elastic deformation of a ball bearing is the Fa : axial bearing load [N] distance that the inner ring moves axially relative to the outer ring when the axial clearance of the ball bearing has been removed and an increasing axial load With a contact angle of 15° (C), the radial stiffness of has been applied. This value does not increase bearing pairs is assumed to be approximately six times as linearly with increasing axial load; rather the contact high as the axial stiffness. With a contact angle of 25° (E), ellipses between balls and raceways become larger as a factor of 2 is assumed. the load increases

Radial elastic deformation

Similarly the radial elastic deformation is caused by a of the ceramic material, these bearings are stiffer than radial load component after radial clearance has been bearings assembled with steel balls. The stiffness of removed. Under otherwise identical conditions, with bearings using balls made of Si_3N_4 is about 30 % higher a small contact angle, the radial elastic deformation is than the stiffness of bearings using steel balls. considerably less than the axial elastic deformation. With an increasing contact angle, the radial yield increases Specific applications must consider the operating while the axial yield decreases until both values become temperature which can affect the bearing clearances. roughly identical at approximately 35°. Likewise, differing thermal expansion coefficients may play a decisive role in bearing material selection.

Both types of deformation depend on the internal geometries of bearing, the existing radial clearance and For further information, please contact your nearest GRW applied load. Sales Representative.

Effect and application

The relatively large amount of yield can be reduced by using preloaded bearing pairs (see chapter "Duplexed bearings"). Preloading will result not only in a reduction of the elastic yield, resulting in increased stiffness, but also in a nearly linear relationship between loading and yield for a considerably wide range of applied loads.

For example: A ball bearing pair with a 10 N preload will maintain linearity up to approximately 30 N of applied axial load. Exceeding this load value will cause the balls to lose contact with the raceway transferring the load to one bearing.



Fv ≈ Fa / 3

- Fv : axial preload [N]

Specific material properties always play an important role. In hybrid bearings using ceramic balls (e.g. Si₃N₄, ZrO₂) the material properties of the ceramic balls should be taken into consideration. Due to the lower elasticity



Relationship between radial play, axial play, contact angle and tilting angle

Radial play

Radial play has minimal effect on the quality of a bearing; however it does have a significant effect on its performance. For example, the bearing's life rating, running noise, vibrations and thermal behavior all depend on the appropriate radial play. (See chapter: "Reduction in radial play")

Radial play is the measurement of the total movement of one ring relative to the other in a plane perpendicular to the bearing axis. In selecting the appropriate radial play, the fit of the bearing on the shaft and in the housing is of particular importance.

Larger than the standard radial play (4-11 µm) should be selected if the ball bearing runs under axial preload and operates at high speeds, or if low torque is required.

Less than standard radial play should be specified if a radial load is applied or low noise is required.

Less than standard radial play is often specified to reduce the axial play in the application. When a very low axial is required we recommend using duplexed bearings (see the chapter "Duplexed bearings").

In deep groove bearings, there is a definite correlation between radial and axial play that is controlled by the internal geometries. For the individual radial play groupings and their respective references, refer to the section titled "Radial Play Classification".

Axial play

The axial play is the measured value in which one bearing ring can move axially in relation to the other with no applied load.

Contact angle

In a load-free condition, the contact angle is called the nominal contact angle. The contact angle is the angle between a plane perpendicular to the ball bearing axis and a line joining the two points where the ball makes contact with the inner and outer raceways. The contact angle of a ball bearing is determined by its radial play, as well as its inner and outer track curvatures.

The contact angle under load is called the operating contact angle. Deformations of a defined size occur at the contact points between balls and raceways. The deep groove radial bearing is a relatively rigid bearing with a very small contact angle range. Here, a highly accurate bearing alignment is of the utmost importance.

Tilting angle

The tilting angle of a bearing is the relative angle to which the inner and outer rings of a bearing can be tilted. The amount of tilting depends on the radial play and the internal geometries of the bearing.

Tilting of the rings should generally be avoided. Even small tilt angles of 2° or 3° may result in increased bearing noise and reduced life. It is critical to place close attention to machining tolerances of mating assembly components to assure proper bearing alignment.

Calibration of bore and outside diameters

To guarantee a uniform fit of bearings on the shaft The following symbols are used for the classification of and in the housing, it is imperative to control diameter graded ball bearings: tolerances of the bearings. It is very difficult to control very small tolerances in a production run; therefore, sorting **Classification of graded bearings** of the rings may be necessary. Only bearings in quality grades P5 and ABEC5 or better can be sorted into groups of 2.5 µm (.0001 inch) or 1.25 µm (.00005 inch). The diameters of the shaft and housing must also be accurately measured and sorted to match.

For technical reasons, it is not possible to supply bearings in only one specific tolerance group. This means that grading to X4, only 3 of 4 possible groups can be contained in the shipment lot, i.e. the final group distribution is subject to production machining variances.

Key to tolerance groups

				Outside diameter D												
	Tolerance field in 0.001 mm			0/-2.5	-2.5/-5	0/-1.25	-1.25/-2.5	-2.5/-3.75	-3.75/-5	0/-1	-1/-2	-2/-3	-3/-4	-4/-5		
		Tolerance field	d in	0/-1	-1/-2	0/5	5/-1	-1/-1.5	-1.5/-2	0/4	4/8	8/-1.2	-1.2/-1.6	-1.6/-2	n gra	
		.0001 inch	Code	1	2	А	В	С	D	E	F	G	Н	l I	giu	ucu
	0/-2.5	0/-1	1	11	512										10	XB
	-2.5/-5	-1/-2	2	21	22										20	ΛD
	0/-1.25	0/5	А			AA	AB	AC	AD						AO	
	-1.25/-2.5	5/-1	В			BA	BB	BC	BD						BO	X4B
	-2.5/-3.75	-1/-1.5	С			CA	СВ 🗸	CC	CD						CO	74D
σ	-3.75/-5	-1.5/-2	D			DA	DB	DC	DD						DO	
Bore	0/-1	0/4	E							EE	EF	EG	EH	EI	EO	
ğ	-1/-2	4/8	F							FE	FF	FG	FH	FI	FO	
	-2/-3	8/-1.2	G							GE	GF	GG	GH	GI	G0	X5B
	-3/-4	-1.2/-1.6	Н							HE	HF	HG	НН	HI	HO	
	-4/-5	-1.6/-2								IE	IF	IG	IH		10	
		not aradad		01	02	OA	OB	0C	OD	OE	OF	0G	OH	OI		0
		not graded		>	(D		Xz	4D				X5D			Symbol	

Different tolerance groups are defined by grading. On the package of each bearing, the relevant group is indicated by means of the following code:

Code BC:
Bore-Ø -1.25/-2.5 μm Outside-Ø -2.5/ -3.75 μr

Method of group classification:

Bore diameter: The smallest measured diameter defines the class



Grading	in groups of 2.5 µm or .0001 inch	in groups of 1.25 µm or .00005 inch	in groups of 1 µm or .00004 inch
Bore d and outside diameter D	Х	X4	X5
Bore d only	ХВ	X4B	X5B
Outside diameter D only	XD	X4D	X5D

Example:

SS624 P5 GPR X4B | LOO1 $X4B = bore graded in 4 groups of 1.25 \mu m$. The outside diameter is not graded.

Code A0:

um

Bore-Ø 0/-1.25 µm Outside-Ø not graded

Code 02: Bore-Ø not graded Outside-Ø -2.5/-5 µm

Outer diameter: The largest measured diameter defines the class.



Reduction in radial play

Ball bearing radial play can increase or decrease during operation due to external influences.

Increases in radial play can cause an increase in contact angle, which distorts the contact ellipse at the transition between raceway and shoulder. This "excessive edge loading" phenomenon may cause premature bearing failure.

In the worst case a reduction in radial play may cause excessive radial preloading of the bearing causing accelerated bearing wear and premature bearing failure.

The following factors have direct influence on changes in radial play:

- Temperature gradients within the bearing or materials with different temperature coefficients.
- Shaft and housing fits.
- Speed related Centrifugal forces.

Reduction in radial play due to thermal expansion

Bearing clearances are set at an ambient temperature of +20 °C which excludes external loads except measuring loads. Frictional heat generation or temperature differentiation between inner and outer rings can very often cause unfavorable environments. The resulting differential expansions of inner ring and outer ring change the radial play. This factor has to be considered when designing the bearing.

$\Delta S_{PT} \approx \Delta d_{q} - \Delta d_{i} - 2\Delta DW$

- ΔS_{PT} : Change in radial play due to thermal expansion [µm]
- Δd_{a} : Change in outer raceway diameter for temperature T [µm]
- Δd_i : Change in inner raceway diameter for temperature T [µm]
- ΔDw : Change in ball diameter for temperature T [µm]

The resultant diameter change caused by the temperature difference is calculated. (Reference: ambient temperature +20 °C):

For the outer ring: $\Delta d_{\alpha} = d_{\alpha 0} \cdot \alpha \cdot \Delta T$

For the inner ring: $\Delta d_i = d_{i0} \cdot \alpha \cdot \Delta T$ For the balls: $\Delta Dw = Dw \cdot \alpha \cdot \Delta T$

d_{a0} : Raceway diameter of outer ring at +20 °C [mm]

d_{i0} : Raceway diameter of inner ring at +20 °C [mm] Dw : Ball diameter at +20 °C [mm]

- α : Linear expansion coefficient [K⁻¹] for 100Cr6 ... 11 · 10⁻⁶ X65Cr13 ... 10.8 · 10⁻⁶ X30CrMoN15-1 ... 10.8 · 10⁻⁶ Si₃N₄... 3.2 · 10⁻⁶ ZrO₂ ... 10.0 · 10⁻⁶
- ΔT : Temperature difference between temperature T and ambient temperature of +20 °C in [K]

Reduction in radial play due to an interference fit

Interference fits cause a reduction in radial play and so the fitting tolerance should be chosen carefully. The reduction in radial play depends on the effective interference fit and the ring thickness ratio. These ratios can be calculated as follows:

ΔS_{RÜI} ≈ k · ü

- $\Delta S_{\textrm{\tiny RII}}$: Reduction in radial clearance due to interference fit [µm]
- : Factor from the table, while it is presumed that the inner ring is pressed onto a complete shaft or the outer ring is pressed into a stable, non-deformable housing.
- : Largest interference fit [µm] Ü

If interference fits are used on the shaft and on the housing, the total reduction in radial play is determined by adding both values.

k-factor for inner ring (IR) and outer ring (OR)

metric									inch		
Basic symbol	IR	OR									
68/1,5/0003	0.4	0.8	694	0.7	0.8	699	0.7	0.8	1016	0.7	0.8
681	0.6	0.8	604	0.6	0.8	609	0.7	0.8	1191	0.6	0.8
691	0.5	0.8	624	0.6	0.8	629	0.6	0.8	1397	0.6	0.8
68/1,5/0001	0.5	0.8	634*	0.5	0.8	6800	0.8	0.9	5/64	0.6	0.8
68/1,5	0.8	0.8	675	0.9	0.8	6900	0.8	0.9	2380	0.8	0.9
69/1,5	0.5	0.8	675/004	0.9	0.8	6000	0.7	0.8	3/32	0.5	0.9
682	0.7	0.8	694/1002	0.9	0.8	6901	0.8	0.9	3175/0002	0.6	0.9
682/005	0.7	0.8	685	0.8	0.8	6001	0.7	0.9	3175	0.8	0.9
692/003	0.6	0.8	685/003	0.8	0.8	6001/003	0.7	0.9	1/8A	0.7	0.9
692	0.6	0.8	695	0.7	0.8	6802	0.9	0.9	3175/6	0.8	0.6
693/0001	0.5	0.9	605	0.6	0.8	6902	0.8	0.9	1/8A/6	0.7	0.7
67/2,35	0.8	0.8	625	0.6	0.8	6002	0.8	0.9	1/8B	0.6	0.9
68/2,35	0.8	0.9	635	0.5	0.8	6803	0.9	0.9	3175/55	0.8	0.5
67/2,5	0.8	0.9	676/003	0.9	0.9	6903	0.8	0.9	3175/6	0.8	0.6
68/2,5	0.7	0.9	695/1202	0.8	0.9	6003	0.8	0.9	3175/8	0.8	0.4
69/2,5	0.6	0.9	686	0.8	0.9	6804	0.9	0.9	1/8B/083	0.6	0.6
683/0001	0.6	0.9	696	0.7	0.8	6904	0.8	0.9	3967	0.7	0.9
60/2,5	0.6	0.8	625/0002	0.7	0.8	6805	0.9	0.9	4763A	0.9	0.9
673	0.8	0.9	626	0.6	0.8				4763B	0.8	0.9
683	0.8	0.9	688A/1322	0.8	0.9				4763A/082	0.9	0.6
683/003	0.8	0.9	687	0.8	0.9				4763B/083	0.8	0.7
693/003	0.7	0.9	697	0.7	0.8				3/16	0.7	0.9
693	0.7	0.9	607	0.7	0.8				6350A	0.9	0.9
683/8	0.8	0.8	627	0.6	0.8				6350B	0.8	0.9
623	0.6	0.8	688A/142	0.9	0.8				1/4A	0.7	0.8
623/13	0.6	0.6	688	0.8	0.9				1/4	0.6	0.8
633	0.5	0.8	688/003	0.8	0.9				7938	0.9	0.9
674	0.9	0.9	698	0.7	0.8				3/8	0.7	0,8
684	0.8	0.9	608	0.7	0.8				12700B	0.9	0.9
684/103	0.8	0.8	689	0.8	0.9				1/2	0.7	0.8
684/10	0.8	0.8	689/003	0.8	0.9				1/2/001	0.7	0.8

Subject to change.



* For a detailed example, refer to page 22.



Reduction in radial play

Reduction in radial play due to centrifugal forces

At very high shaft speeds or inner ring rotation, the centrifugal forces of the rotating parts increase. The load on the outer ring and the balls also increases and the inner ring expands. The expansion of the inner ring changes the fit of the shaft and bearing and the bearing may begin to slip on the shaft. In this situation, a tighter fit must be selected. These types of deformations depend on the bearing size, retainer, balls, materials used, and inner geometry of the bearing.

Please contact our sales engineers to find out more about the reduction in radial play due to centrifugal forces.

Example:

The ball bearing SS634-2Z GPR J (d = 4 mm, D = 16 mm, Dw = 2.50 mm, material of rings and balls: X65Cr13) is to run in an application at 35,000 1/min. During the operating phase, the temperature at the inner ring is +60 °C and at the outer ring +30 °C. The ball bearing is mounted on the shaft with a press fit j5 (+3/-2) and in the housing with a tight fit K5 (+2/-6).

Change in radial clearance due to thermal expansion:

Outer ring:

 $d_{a0} \approx (d+D)/2 + Dw = (4+16) \text{ mm}/2 + 2.50 \text{ mm} = 12.50 \text{ mm}$ $\Delta d_{a} \approx d_{a0} \cdot \alpha \cdot \Delta T = 12.500 \text{ mm} \cdot 10.8 \cdot 10^{-6} \text{ 1/K} \cdot 10 \text{ K} = 1,35 \text{ µm}$ Inner ring: $d_{i0} \approx (d+D)/2 - Dw = (4+16) \text{ mm}/2 - 2.50 \text{ mm} = 7.50 \text{ mm}$ $\Delta d_{i} \approx d_{i0} \cdot \alpha \cdot \Delta T = 7.50 \text{ mm} \cdot 10.8 \cdot 10^{-6} \text{ 1/K} \cdot 40 \text{ K} = 3.24 \text{ µm}$ Ball: Dw = 2.50 mm

 $\Delta Dw \approx Dw \cdot \alpha \cdot \Delta T = 2.50 \text{ mm} \cdot 10.8 \cdot 10^{-6} \text{ } 1/\text{K} \cdot (10+40) \text{ } \text{K}/2 \approx 0.68 \text{ } \text{\mu}\text{m}$

Change in radial clearance due to thermal expansion:

$$\begin{split} \Delta S_{\text{RT}} &\approx \Delta d_a - d_{i0} - 2\Delta Dw \\ \Delta S_{\text{RT}} &\approx (1.35 - 3.24 - 2 \cdot 0.68) \, \mu\text{m} = -3.25 \, \mu\text{m} \end{split}$$

The radial clearance is reduced due to the temperature difference between inner ring and outer ring by $3.25 \ \mu m$.

Change in radial clearance due to interference fit:

Outer ring:

Outside diameter: $0/-8 \ \mu m$ Housing diameter: $+2/-6 \ \mu m$ $\Delta S_{RUa} \approx k \cdot U$ $\Delta S_{RUa} \approx 0.8 \cdot 6 \ \mu m = 4.8 \ \mu m$

Inner ring:

Bore: $0/-8 \ \mu m$ Shaft: $+3/-2 \ \mu m$ $\rightarrow \ddot{u} = 11 \ \mu m$ $\Delta S_{R\ddot{U}_i} \approx k \cdot \ddot{u}$ $\Delta S_{R\ddot{U}_i} \approx 0.5 \cdot 11 \ \mu m = 5.5 \ \mu m$ The raidal clearance changes due to the interference fit by 4.8 \ \mu m + 5.5 \ \mu m = 10.3 \ \mu m

Total change of radial clearance due to thermal expansion and interference fit:

$$\begin{split} \Delta S_{\text{R}} &= \Delta S_{\text{RT}} + \Delta S_{\text{RU}} \text{ [µm]} \\ \Delta S_{\text{R}} &= 3.25 \text{ µm} + 10.3 \text{ µm} = 13.55 \text{ µm} \end{split}$$
 This total reduction in radial clearance must be considered when selecting the radial clearance of the bearing.

Radial play classification

Radial play for deep groove radial bearing

d	max 6 mm	
C2	0 to 6 µm	
CN	4 to 11 µm	
C3	10 to 20 µm	
C4	14 to 20 µm	
C5	18 to 28 µm	

d r	nore than 6 to 10 mm	
C2	0 to 6 µm	
CN	4 to 11 µm	
C3	10 to 20 µm	
C4	14 to 29 µm	
C5	20 to 37 µm	

d	more than 10 to 18 mm	
C2	O to 9 µm	
CN	3 to 18 µm	
C3	11 to 25 μm	
C4	18 to 33 µm	
C5	25 to 45 µm	

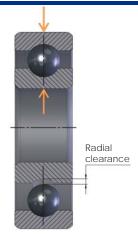
d	more than 18 to 24 mm	
C2	0 to 10 µm	
CN	5 to 20 µm	
C3	13 to 28 µm	
C4	20 to 36 µm	
C5	28 to 48 µm	

The standard radial play is not indicated in the ball bearing numbering system.

Deviating radial clearance data metric system

C1/5	1 to 5 µm
C4/8	4 to 8 µm
C7/11	7 to 11 µm
C10/15	10 to 15 µm





d	more	tha	n 24 to 30 mm
C2		1	to 11 µm
CN		5	to 20 µm
C3		13	to 28 µm
C4		23	to 41 µm
C5		30	to 53 µm

d more than 30 to 40 mm

C2	l to ll µm
CN	6 to 20 µm
C3	15 to 33 µm
C4	28 to 46 µm
C5	40 to 64 µm

d more than 40 to 50 mm

C2]	to 11 µm
CN	6	to 23 µm
C3	18	to 36 µm
C4	30	to 51 µm
C5	45	to 73 µm

Deviating radial clearance data inch system

KO2	0" to .0002"
K13	.0001″ to .0003″
K24	.0002" to .0004"
K35	.0003″ to .0005″
K46	.0004" to .0006"
K58	.0005″ to .0008″



Functional tests

There are different functional tests that can be performed by GRW. As a standard, 100% of our ball bearings are noise tested. Besides this standard testing, the following tests are available: axial vibration tests, torque test and preload measurement.

These tests ensure the uniformity of the production run and compliance with customer requirements. All functional tests carried out by GRW take place in a class R 10,000 cleanroom (ISO 14644-1, class 7).

The functional test method is always selected to simulate the intended use of the bearing.

Noise test GPR

In the GRW numbering system GPR designates 100% noise testing. Using highly sensitive noise testing equipment, the amplitude of the vibrations generated by the miniature bearings is measured at specified speeds and frequencies. This method detects imperfections, such as ball or raceway defects and isolates their root cause

This noise test is carried out in a class R10.000 cleanroom in accordance with ISO 14644-1, class 7. A standard reference oil is used to eliminate the variable effects of different lubricants

Axial vibration test GPA

GPA stands for noise testing in the axial direction. Similar to the GPR test, the axial vibrations measured by the GPA vibration meter identify the shape and surface properties of raceways and balls in the bearings.

GPA testing measures vibration noise in four distinct frequency ranges as compared to two frequency ranges for the GPR test. The amount of movement or 'peak to peak displacement' value is also recorded. The cumulative total of these distinct measurements provides a direct understanding of the ball bearing's running behavior.

As with the GPR test, standard reference oil is used to eliminate the variable effects of different lubricants.

The GPA test is offered at an additional charge. If you require any further information, please contact your GRW sales representative.

Torque test

GRW uses different methods to measure starting and dynamic torque. The Asch testing device due to MIL-STD-206 provides very exact and reliable starting torque values. During this test the outer ring is driven and the inner ring is loaded relative to each bearing size. The standard axial loading of the inner ring is 75 g for ball bearings with an outer diameter of up to 10 mm. Ball bearings with a larger outer diameter (> 10 mm) are loaded with 400 g.

Since there is no universally accepted standard for torque measurement, the torques of identical bearings can only be compared if they have been measured under the same measuring conditions with the same measuring devices.

Table "maximum starting torque in µNm" shows reference values for the maximum starting torque. These values apply for instrument ball bearings without seals, P5 or ABEC5 or better, which are lubricated with instrument oil having a low viscosity $\leq 14 \text{ mm}^2/\text{s}$ at +40 °C. The values can be 10 to 40 times higher for ball bearings with grease lubrication.

Running or dynamic torque is the force required to keep a bearing in rotation. A special dynamic torque tester developed by GRW for this very purpose is available on request to measure the running torque at higher speeds.

Maximum starting torque in µNm

Basic	Torque	Load	Basic	Torque	Load	Basic	Torque	Load
symbol	in [µŃm]	in [g]	symbol	in [µÑm]	in [g]	symbol	in [µÑm]	in [g]
681	15	75	695	69	400	1016	15	75
691	15	75	605	69	400	1191	15	75
68/1,5	15	75	625	69	400	1397	15	75
69/1,5	15	75	635	76	400	5/64	15	75
682	15	75	686	69	400	2380	15	75
692	15	75	696	69	400	3/32	15	75
67/2,35	15	75	626	76	400	3175	15	75
68/2,35	15	75	687	69	400	1/8A	15	75
68/2,5	15	75	697	76	400	1/8B	16	75
69/2,5	15	75	607	76	400	3967	15	75
60/2,5	16	75	627	80	400	4763A	15	75
673	16	75	688A	52	400	4763B	16	75
683	16	75	688	76	400	3/16	52	400
693	16	75	698	76	400	6350A	15	75
623	16	75	608	80	400	6350B	52	400
674	16	75	689	76	400	1/4A	60	400
684	16	75	699	80	400	1/4	70	400
694	65	400	609	80	400	7938	52	400
604	65	400	629	100	400	3/8	95	400
624	69	400	6800	80	400			
634	69	400	6900	95	400			
675	65	400	6000	100	400			
685	65	400						

Conversion table

	1 μNm =	1 cmp =	1 oz.in. =	1 cNcm =
μNm	1	100	7200	100
стр	0.01	1	72	1
oz.in.	0.000139	0.0139	1	0.0139
cNcm	0.01	1	72]

Assembly of low-torque ball bearings

Extreme cleanliness of parts and assembly area is essential to produce a perfect low-torque bearing. Even the tiniest Shaft and housing fits and tolerances for low-torque contaminations of the ball bearings can cause torque bearings are particularly important. Shaft and housing peaks, which may be many times higher than the average tolerances need to be selected so that they result in a torque level. sliding fit. Please refer to the chapters "Fitting Tolerances" and "Reduction in radial play".

Even a small misalignment of the inner or outer ring can result in an increased bearing torque. Particular attention Another testing device specifically developed by GRW measures and records the preloading of duplexed must be given to the exact alignment between shaft and housing bore, as well as to the parallelism of the bearings (following the "broken curve" method). This type mating faces. of measurement is available on request.



Preloading test



Tolerance and Runout Tables – inner ring

(International Organization for Standardization) and ABEC bearings according to ABEC quality standards ABEC1 to standards (Annular Bearing Engineering Committee). For ABEC9 (ABEC9 = highest tolerance). metric size bearings, tolerances comply with ISO quality

GRW bearings conform to the applicable ISO PO to P2 (P2 = highest tolerance) and for inch size

GRW manufactures miniature ball bearings according to Including tolerances of mating parts, such as shafts and the highest quality standards for both inch and metric sizes. housings, to create a bearing friendly environment. GRW's sales engineers will be pleased to support you selecting the suitable quality for your application.

Definition:		Diameter	d [mm]		PO [µm]		Ρ6 μm]	P5 [µm]		P4 [µm]	P2 [µm		P5A (4) [µm]		4A (4) [µm]	P4 9			EC1 1 inch]		EC3		BEC5		EC7		EC9 1 inch]		C3P 1 inch]		EC5P		EC7P	ABEC9F		ABEC5T (6) [.0001 inch]
		series	above	to ma												. max.		max.	min.		min.		. min.			max.		max.			min.		-	max. mi		max. min.
single plane mean			0.6 1	8 0	-8	0	-7 (C	5 0	-4	0	-2.5	0.	-5 0	-2	1 0	-4	0	-3	0	-3	0	-2	0	-1.5	0	-]	0	-2	0	-2	0	-2	0 -	-1 (0 -2
bore diameter	∆dmp			0 0	-10		-8 (С	60	-5		-2.5	0 .	-6 0		5 0	-5	0	-4	0	-3	0	-2.5	0	-2	0	-]	0	-2	0	-2	0	-2	0 .	-1 (0 -2
deviation				0 0		0	-10 (C	8 0	-6	0	-2.5				0	-6	0	-4.5	0	-4	0	-3	0	-2.5	0	-]								(0 -3
				8 10		9		5	4		2.5		3	2.5		2.5														1		1		.5		
		7/8/9		0 13		10		5	5		2.5		3	2.5		2.5														1]		.5		
				0 13		13	5	8	6		2.5		0	0.5		2.5																			\rightarrow	
Bore diameter variation	Valara	0		8 8		/	4	4 5	3		2.5		3	2.5 2.5		2.5 2.5														1		1		.5		
in a single radial plane (out of roundness)	Vdsp	0		0 10		8 10		5	4		2.5 2.5		3	2.5		2.5														I		I		.5		
			-	8 6		5		4	3		2.5		3	2.5		2.5														1		1		.5	—	
		2/3		0 8		6	-	+ 5	4		2.5		3	2.5		2.5														1		1		.5		
		27 0		0 9		8		5	5		2.5		0	2.0		2.5																		.0		
			-	8 6		5		3	2		1.5		3	2		1.5														1		1		.5	-	
Mean bore diameter	Vdmp			0 8		6	:	3	2.5		1.5		3	2.5		1.5														1		1		.5		
variation (conicity)			30 5	0 9		8	2	4	3		1.5					1.5																				
			0.6 2.	5 0	-40	0	-40 () -4	0 0	-40	0	-40	0 -2	5 0	-25	5 0	-100																			
			0.6 1	0														0	-50	0	-50	0	-16	0	-16	0	-16	0	-50	0	-10	0	-10	0 -1	0	
Variation of a single inner ring width from	$\Delta Bs^{(1)}$		2.5 1	0 0			-120 (0 0	-40	0	-40		5 0			-100																			
nominal dimension	200			8 0			-120 (0 0	-80		-80		5 0			-100	0	-50	0	-50	0	-32	0	-32	0	-32	0	-50	0	-10	110	-10		12 1	0 -10
				0 0			-120 (0 0	-120		-120	0 -2	5 0	-25		-120	0	-50	0	-50	0	-50	0	-50	0	-50	0	-50	0	-10	0	-10	0 -1		0 -10
				0 0			-120 (0 0	-120		-120					-120	0	-50	0	-50	0	-50	0	-50	0	-50									0 -50
			0.6 2.		2	12		5	2.5		1.5					1.5		,		,				1		F			11	0			and the second	F		
				0 13	5	15		5	0.5		15		5	2.5		1.5		6		6		2				.5		/		2			AT BB	.5		
Variation in the width of the inner ring	VBs			8 20		15 20		5	2.5 2.5		1.5 1.5		5	2.5		1.5		Q		Q		2		1		5		11		2	and the second second	1		.5		2
				0 20		20		5	2.5		1.5		5	2.5		1.5		8		8		2		1		.5				2		1		.5	Ń	2
				0 20		20		5	3		1.5		0	2.0		1.5		8		8		2		1		.5	12			S.					35	2
				.5 10		5	4	4	2.5		1.5		3.5	2.5		1.5		3		2.5		1.5		1		.5		2	- A	1.5	-	1		.5	É	AAA
Radial runout of the				0 10		6	4	4	2.5		1.5		3.5	2.5		1.5		3		2.5		1.5		1		.5		2		1.5		1	12 3	.5	NA	XXX
inner ring of the	Kia		10 1	8 10)	7	4	4	2.5		1.5		3.5	2.5		1.5		4		3		1.5		1		.5		2		1.5	- NEL	15	BACI	.5	NP	2
assembled bearing (dynamic imbalance)			18 3	0 13	3	8	4	4	3		2.5		3.5	3		2.5		5		3		1.5		1		1		3		1.5	1	1.5	CP -	NR	JA.	2
			30 5	013	5	10	1	5	4		2.5					2.5		6		4		2		1.5	l	/1		1			AR	A	TR	S		3
E. I. M. I.			0.6 1				-	7	3		1.5		7	3		1.5						3		1		.5				3	A	TH	XV	.5		3
Face runout with bore (lateral runout)	Sd		18 3				5	8	4		1.5		8	4		1.5						3		1.5		.5				3	KAL I	1.5	Y	.5		3
			30 5	_			8	8	4		1.5			_		1.5						3		1.5	A	.5	1			7AB	411	X	200			3
Assembled bearing inner	_		0.6 1				-	7	3		1.5		7	3		1.5						3		1	11	.5				3	77	SV		.5		3
ring face runout with raceway (axial runout)	Sia			0			8	8	4		2.5		8	4		2.5						3		1.5						3	CH4	1.5		.5		3
			30 5	0		1	8	8	4		2.5					2.5						3		1.5	1	1				17	TAT					3

Subject to change.

⁽¹⁾ Tolerance for matched bearings is 0/-200 µm

⁽²⁾ Applicable before assembly of the bearing and after removal of the inner and/ or outer circlips

⁽³⁾ For flanged bearings inboard side of the flange ⁽⁴⁾ For deep groove radial bearings only



⁽⁵⁾ For spindle bearings only⁽⁶⁾ Nominal value for bores of 9 mm and up

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Tolerance and Runout Tables – outer ring

Definition:		Diameter	D [mm]	ΡΟ [μm]		P6 [µm]	P5 [µm]	P ⁄ [µr		P2 [µm]	P5A (* [µm]		A (4) Jm]	P4S [µn			BEC1 001 inch]		BEC3		SEC5 D1 inch]		SEC7 D1 inch]		EC9	ABE [.0001		ABEC		ABEC		ABEC9 [.0001 inc		ABEC5T (6 [.0001 inch]	
		series				ax. min. I									, min.	max			. min.	max.	min.	-	min.		min.	max.	-	max.		-		max. m		max. min.	
Single plane mean outside diameter deviation	∆Dmp		18 30 30 50		-8 0 -9 0 11 0 13 0	-8	0 · 0 ·	-5 0 -6 0 -7 0 -9 0	-4 0 -5 0 -6 0) -4) -4	0	-5 0 -6 0 -7 0	-4 -5 -6	0	-4 -5 -6 -7	0 0 0	-3 -4 -5 -5	0 0	-3 -3 -4 -4.5	0 0 0	-2 -2 -3 -3.5	0	-2 -2 -2.5 -3	0 0 0	-1 -1.5 -1.5 -1.5	0 0 0	-3 -3 -3	0 0 0	-2 -2 -2	0 0 0		0 0 -1 0 -1	.5 (0 -2 0 -4 0 -4	2 1 1
		7/8/9	18 30	14	1	0	5 6 7 9	4 5 6 7	2 4 4 4	2.5 - -	3 3 3	2.5 2.5 2.5		2.5 4 4 4]]]]]]		.5 .8 .8			
Outside diameter variation in a single radial plane (out of roundness)	VDsp ⁽²⁾	0	2.5 1 18 30	8 8 0 9 0 11	7 8 9		4 5 5 7	3 4 5 5	2 4 4 4	2.5 - -	3 3 3	2.5 2.5 2.5		2.5 4 4 4]]]]]]		.5 .8 .8			_
		2/3	18 30	3 6 7 7 8 10	5 6 7 8	· · · · · ·	4 5 5 7	3 4 5 5	2 4 4 4	2.5 - -	3 3 3	2.5 2.5 2.5		2.5 4 4 4]]]		1 1 1		.5 .8 .8			
Mean outside diameter variation (conicity)	VDmp ⁽²⁾		18 30	3 6 0 7 0 8 0 10	5 6 7 8		3 3 4 5	2 2.5 3 3.5	1 2 2 2	.5	3 3 4	2 2.5 3		1.5 2 2 2]]]]]]		.5 .8 .8			
Variation of a single outer ring width from nominal dimension	$\Delta Cs^{(1)}$		2.5 1 18 30 30 50 50 80)))	entical	with Bs for	inner ring	g of the s	ame bec	aring	0 -: 0 -:	25 0 25 0	-25 -25	0	-120 -120 -150	0 0 0	-50 -50 -60	0	-50 -50 -60	0 0 0	-50 -50 -60	0	-50 -50 -60	0 0 0	-50 -50 -60	0 0	-50 -50	0 0	-10 -10	0			10 0	0 -10 0 -10 0 -50)
Variation in width	VCs		2.5 13 18 30 30 50 50 80)))	ntical v	with VBs for	inner rin	g of the s	same be	earing	5 5	2.5 2.5		1.5 1.5 1.5		8 8 10		8 8 10		2 2 2.5]]]		.5 .5 .5				2 2]]		.5 .5		2 2 2	
Radial runout of outer ring of assambled bearing (dynamic imbalance)	Кеа		18 30 30 50	3 15 0 15 0 20 0 25		0	5 6 7 8	3 4 5 5	2	.5 2.5 2.5	5 6 7	3 4 5		1.5 2.5 2.5 4		6 6 8 10		4 4 5		2 2 3 3		1.5 1.5 2 2		.5 1 1 1.5		4 4 4		2 2 2		1.5 1.5 2		.5 1 1		2 3 3	
Variation of the outside surface generatrix inclination with face ⁽³⁾ (lateral rounout)	SD		2.5 80				8	4	1	.5	8	4		1.5						3		1.5		.5				3		1.5		.5		3	
Assembled bearing outer ring face flange back face rounout with racewa (axial runout)	Sea Iy		2.5 18 18 30 30 50 50 80				8 8 8 10	5 5 5 5	2	.5 2.5 2.5	8 8 8	5 5 5		1.5 2.5 2.5 4						3 3 3 5		2 2 2 2		.5 1 1 1.5				3 3 3		2 2 2		.5 1 1		3 3 4	No.
Assembled bearing outer ring face flange back face rounout of assembled bearing	Seal		2.5 13 18 30 30 50 50 80				11 11 11 11	7 7 7 7	3 4 4	}	10 10 10	7 7 7															AN A	3 3 3		3 3 3		N			X
Variation of a single outside diameter of outer ring Flange diameter is used for positioning	∆FD		10 1 18 30 30 50	3 0 - 0 0 - 0 0 -	36 0 43 0 52 0 62 0 74 0	-43 -52 -62	0 -4 0 -5 0 -6	6 0 .3 0 .2 0 .2 0 .2 0 .4 0	-36 0 -43 0 -52 0 -62 0 -74) -43) -52	0 -	25 0 25 0 25 0 25 0 25 0	-25 -25 -25 -25													50 50 50 50	-20 -20 -20 -20	0	1	0000	-10 -10 -10 -10		222	JSEX.	¥
Variation of a single width outer ring flange from nominal dimension	∆FB		2.5 10 10 13 18 30 30 50	0 -1 3 0 -1 0 0 -1 0 0 -1 0 0 -1	20 0 20 0 20 0 20 0 20 0	-120 -120 -120 -120	0 -4 0 -8 0 -12 0 -12	0 0 0 0 0 0	-40 C -80 C) -80) -120	0 0	40 0 50 0 50 0 50 0	-40 -50 -50 -50													0 0 0	-20 -20 -20 -20		-20 -20	00000	-20 -20 -20 -20				

Subject to change. ⁽¹⁾ Tolerance for matched bearings is 0/-200 µm



⁽⁵⁾ For spindle bearings only
 ⁽⁶⁾ Nominal value for bores of 9 mm and up

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GRW- designation	Main dim [m [in	nensions in I m] Ich]	Width	aring without clo Width with	Flange d	limensions	Width with	aring with clos Width with	Flange d	limensions	Chamfer in [mm] [inch]	acc. to	g dimensions DIN 5418 mm]		ngs acc. to) ⁽²⁾ (max)	Closure	options ⁽³⁾	Max. limiting sp	beed ⁽⁵⁾ [mm ⁻¹]
			without closure	extended inner ring without closure	without	t closure	closure	extended inner ring with closure	with c	closure		Shaft diameter	[inch] Housing diameter						
Basic symbol	d	D	В	B ₁	Flange diameter FD	Flange width FB	B ₂	B ₃	Flange diameter FD ₁	Flange width FB ₁	r _{s min} (1)	d _{a min}	D _{a max}	C _r [N]	C _{or} [N]	Shield ⁽⁴⁾	Seal ⁽⁴⁾	without closure or with shield	with seal
67/0,6	0.60	2.00	0.80	-	-	-	-	-	-	-	0.05	1.00	1.60	27	7	_	-	170000	-
	.0236	.0787	.0315								.002	.039	.063	1/0				10000	
8/1,5/0003	0.80	4.00	2.00	-	5.00	0.60	2.00	-	5.00	0.60	0.05	1.20	3.60	163	44	Х	-	138000	-
81	.0315 1.00	.1575 3.00	.0787 1.00	-	.1969	.0236	.0787 2.00	-	.1969	.0236	.002 0.05	.047 1.40	.142 2.60	82	22	X	_	150000	_
	.0394	.1181	.0394	-	-	-	2.00 .0787	-	-	-	.002	.055	.102	02	22	^	_	130000	_
81/003	1.00	3.00	2.00	_	-	-	2.00	-	_	_	0.05	1.40	2.60	52	21	Х	_	170000	_
,017,000	.0394	.1181	.0787				.0787				.002	.055	.102	02	21			17 0000	
091	1.00	4.00	1.60	-	-	-	2.30	-	-	-	0.10	1.60	3.40	160	43	_	_	126000	_
	.0394	.1575	.0630				.0906				.004	.063	.130						
8/1,5/0001	1.00	4.00	-	-	-	-	2.00	-	5.00	0.60	0.05	1.40	3.60	163	44	Х	-	130000	-
	.0394	.1575					.0787		.1969	.0236	.002	.055	.142						
8/1,5/0011	1.00	4.00	2.00	-	5.00	0.60	2.00	-	-	-	0.05	1.40	3.60	163	44	Х	-	130000	-
	.0394	.1575	.0787		.1969	.0236	.0787				.002	.055	.142						
8/1,5	1.50	4.00	1.20	2.00	5.00	0.40	2.00	-	5.00	0.60	0.05	1.90	3.60	163	44	Х	-	153000	-
	.0591	.1575	.0472	.0787	.1969	.0157	.0787		.1969	.0236	.002	.075	.142						
08/1,5A	1.50	4.00	-	-	-	-	2.00	-	5.00	0.60	0.05	2.10	3.60	112	33	Х	-	120000	-
	.0591	.1575	.0787				.0787		.1969	.0236	.002	.083	.142						
9/1,5 (4)	1.50	5.00	2.00	2.80	6.50	0.60	2.60	3.40	6.50	0.80	0.15	2.30	4.20	192	59	Х	-	109000	-
	.0591	.1969	.0787	.1102	.2559	.0236	.1024	.130	.2559	.0315	.006	.091	.165						
9/1,5/002	1.50	5.00	-	-	-	-	2.00	-	6.50	0.60	0.15	2.30	4.20	192	59	X	-	93000	
0 /1 5	.0591	.1969	0.50		7.50	0.70	.0787		.2559	.0236	.006	.091	.165		00	/ //////		00000	A Pratici
0/1,5	1.50 .0591	6.00 .2362	2.50 .0984	-	7.50 .2953	0.60 .0236	3.00 .1181	-	7.50 .2953	0.80 .0315	0.15 .006	2.30 .091	5.20 .205	330	98	Х	-	90000	-
572	2.00	4.00	1.20	_	.2933	.0230	2.00	_	.2933	.0313	0.05	2.40	3.60	124	40	V		104000	
/ Z	.0787	.1575	.0472	_	-	_	.0787	-	_	_	.002	.094	.142	124	40	A		104000	THE .
82	2.00	5.00	1.50	2.30	6.10	0.50	2.30	3.10	6.10	0.60	0.08	2.50	4.50	192	59	X	Х	116000	71000
02	.0787	.1969	.0591	.0906	.2402	.0197	.0906	.122	.2402	.0236	.003	.098	.177	172	37	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	110000	/1000
32/003	2.00	5.00	_	-	-	-	2.50	-	6.20	0.60	0.10	2.60	4.40	169	50 /	Х	- <u>11-12</u>	100000	H tot
	.0787	.1969					.0984		.2441	.0236	.004	.102	.173				122	JCN RX	Alses
82/005	2.00	5.00	2.60	-	6.50	0.80	2.60	-	6.50	0.80	0.08	2.50	4.50	192	59	Х	-	105000	-
	.0787	.1969	.1024		.2559	.0315	.1024		.2559	.0315	.003	.098	.177						
92/003	2.00	6.00	2.00	-	-	-	-	-	-	-	0.15	2.80	5.20	286	90	- 1	KIFIK	91000	-
	.0787	.2362	.0787								.006	.110	.205	n -		X	ALLA		
92	2.00	6.00	2.30	3.10	7.50	0.60	2.30	3.10	7.50	0.60	0.15	2.80	5.20	286	90	Х	Х	91000	65000
	.0787	.2362	.0906	.1220	.2953	.0236	.0906	.122	.2953	.0236	.006	.110	.205						

Note:

(1) f_{s min} = minimum single bearing chamfer or maximum permissible shaft or housing fillet radius
 (2) Other load ratings are possible with different ball complements and non standard retainers
 (3) Different shields and seals are available

⁽⁴⁾ Bearings also available with 1 or 2 shields/seals
 ⁽⁵⁾ Limiting speed also depends on seal, material and the respective ball complement

• Bearings without shields or retainers are also available with recesses.

Please discuss your desired design in terms of flange, extended inner ring width, shield, lubrication, and material with our Technical Application Consultants to check availability.



• Subject to change.

Almost all bearing types can also be enhanced with GRW XTRA. Detailed information you can find on page 79 and following.



GRW- designation	Main dima [m [inc	m]	Bea Width without closure	ring without clo Width with extended inner ring without closure		imensions		aring with closu Width with extended inner ring with closure	ure in [mm] [i Flange di with c	imensions	Chamfer in [mm] [inch]	acc. to	g dimensions DIN 5418 [mm] [inch] Housing diameter		ngs acc. to) ^[2] (max)	Closure	options ⁽³⁾	Max. limiting sp	peed ⁽⁵⁾ [mm ⁻¹]
Basic symbol	d	D	В	B ₁	Flange diameter FD	Flange width FB	B ₂	B ₃	Flange diameter FD ₁	Flange width FB ₁	r _{s min} (1)	d _{a min}	D _{a max}	C _r [N]	C _{or} [N]	Shield ⁽⁴⁾	Seal ⁽⁴⁾	without closure or with shield	with seal
692/005	2.00	6.00	2.50	-	7.20	0.60	2.50	-	-	-	0.15	2.80	5.20	330	99	Х	-	90000	-
	.0787	.2362	.0984		.2835	.0236	.0984				.006	.110	.205						
92/004	2.00	6.00	3.00	-	7.50	0.80	3.00	-	7.50	0.80	0.15	2.80	5.20	330	99	Х	-	95000	-
11	.0787	.2362	.1181		.2953	.0315	.1181		.2953	.0315	.006	.110	.205						
83/0003	2.00	7.00	3.00	-	8.20	0.60	3.00	-	8.20	0.60	0.15	2.80	6.20	386	129	Х	-	75000	-
	.0787	.2756	.1181		.3228	.0236	.1181		.3228	.0236	.006	.110	.244						
93/0001	2.00	8.00	4.00	-	9.50	0.90	4.00	-	9.50	0.90	0.15	2.80	7.20	644	215	Х	-	67000	-
7 (0,05 (4)	.0787	.3150	.1575		.3740	.0354	.1575		.3740	.0354	.006	.150	.283	100	50	N/		100000	
07/2,35 (6)	2.35	5.00	1.50 .0591	2.30	6.10	0.50	2.30	-	6.10	0.60	0.08 .003	2.50 .098	4.50 .177	192	59	Х	-	120000	-
0 / 0 0 5 (6)	.0925	.1969		.0906	.2402	.0197	.0906		.2402	.0236				286	90			91000	
8/2,35 (6)	2.35 .0925	5.50 .2165	2.00 .0787	-	-	-	-	-	-	-	0.08 .003	2.90	5.00 .197	280	90	-	_	91000	-
7/2,5	2.50	5.00	1.50	_	-	_	_	_	-	_	0.08	2.90	4.60	192	59	_	_	93000	_
0//2,0	.0984	.1969	.0591	_	-	_	_	_	-	_	.003	.114	.181	172	57			73000	
68/2,5	2.50	6.00	1.80	2.60	7.10	0.50	2.60	3.40	7.10	0.80	0.08	3.00	5.50	286	90	Х	X	101000	61000
5072,5	.0984	.2362	.0709	.1024	.2795	.0197	.1024	.1303	.2795	.0315	.003	.118	.217	200	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	~	~	101000	01000
59/2,5/002	2.50	7.00	.0/0/		.2773	-	2.50		.2770	.0010	0.10	3.10	6.40	177	58	Х	_	75000	
577 2,07 002	.0984	.2756					.0984				.004	.122	.252	177	00	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		10000	
69/2,5	2.50	7.00	2.50	-	8.50	0.70	3.50	-	8.50	0.90	0.15	3.30	6.30	432	149	Х	Х	87000	53000
., _,-	.0984	.2756	.0984		.3346	.0276	.1307		.3346	.0354	.006	.130	.248						
583/0001	2.50	7.00	2.00	-	8.10	0.50	3.00	-	8.10	0.80	0.10	3.60	6.40	432	149	X //		88000	-
	.0984	.2756	.0787		.3189	.0197	.1181		.3189	.0315	.004	.142	.252			/ ////			
50/2,5	2.50	8.00	2.80	3.60	9.50	0.70	2,80	3.60	9.50	0.70	0.15	3.30	7.20	432	149	Х	Х	81000	53000
	.0984	.3150	.1102	.1417	.3740	.0276	.1102	.1417	.3740	.0276	.006	.130	.283						
50/2,5/004	2.50	8.00	4.00	-	9.50	0.90	4.00	-	9.50	0.90	0.15	3.30	7.20	552	177	X	-	71000	
	.0984	.3150	.1575		.3740	.0354	.1575		.3740	.0354	.006	.130	.283			- A		100	To and
573	3.00	6,00	2.00	-	7.20	0.60	2.00	-	-	-	0.08	3.60	5.40	208	74	х	-	81000	-
	.1181	.2362	.0787		.2835	.0236	.0787				.003	.142	.213						
573/003	3.00	6.00	-	-	-	-	2.50	-	7.20	0.60	0.10	3.60	5.40	208	74	Х	-/10	80000	HALLY
	.1181	.2362					.0984		.2835	.0236	.004	.142	.213				123	LLNR S	Star
83/63	3.00	7.00	-	-	-	-	3.00	3.80	-	-	0.10	3.60	7.40	432	149	Х	Х	80000	50000
	.1181	.2751					.1181	.1496			.004	.142	.291						
83	3.00	7.00	2.00	2.80	8.10	0.50	3.00	3.80	8.10	0.80	0.10	3.60	6.40	432	149	X	XXX	90000	53000
	.1181	.2756	.0787	.1102	.3189	.0197	.1181	.1496	.3189	.0315	.004	.142	.252	M			THIN		
83/8	3.00	8.00	3.00	-	-	-	3.00	3.80	-	-	0.10	3.60	7.40	432	149	Х	Х	95000	55000
	.1181	.3150	.1181				.1181	.1496			.004	.142	.291						

Note:

(1) f_{s min} = minimum single bearing chamfer or maximum permissible shaft or housing fillet radius
 (2) Other load ratings are possible with different ball complements and non standard retainers
 (3) Different shields and seals are available

⁽⁴⁾ Bearings also available with 1 or 2 shields/seals

⁽⁵⁾ Limiting speed also depends on seal, material and the respective ball complement ⁽⁶⁾ Tolerance of bore +12µm to 3µm

• Bearings without shields or retainers are also available with recesses.

 Almost all bearing types can also be enhanced with GRW XTRA. Detailed information you can find on page 79 and following. Please discuss your desired design in terms of flange, extended inner ring width, shield, lubrication, and material with our Technical Application Consultants to check availability.





GRW- designation	Main dim [m [in	m]	Width	ring without clo Width with	Flange d	imensions	Width with	aring with clos Width with	Flange d	imensions	Chamfer in [mm] [inch]	acc. to [n	dimensions DIN 5418 nm]		gs acc. to ⁽²⁾ (max)	Closure	options ⁽³⁾	Max. limiting sp	Deed ⁽⁵⁾ [mm ⁻¹]
			without closure	extended inner ring without closure	without	t closure	closure	extended inner ring with closure	with c	closure		(i Shaft diameter	nch] Housing diameter						
Basic symbol	d	D	В	B ₁	Flange diameter FD	Flange width FB	B ₂	B ₃	Flange diameter FD ₁	Flange width FB ₁	r _{s min} (1)	d _{a min}	D _{a max}	C _r [N]	C _{or} [N]	Shield ⁽⁴⁾	Seal ⁽⁴⁾	without closure or with shield	with seal
683/003	3.00	7.00	2.50	-	-	-	2.50	-	-	-	0.10	3.60	6.40	432	149	Х	-	93000	-
- No 200	.1181	.2756	.0984				.0984				.004	.142	.252						
93/003	3.00	8.00	2.50	-	-	-	-	-	-	-	0.15	3.80	7.20	644	215	-	-	60000	-
	.1181	.3150	.0984								.006	.150	.283						
593 (4)	3.00	8.00	3.00	3.80	9.50	0.70	4.00	4.80	9.50	0.90	0.15	3.80	7.20	644	215	Х	Х	80000	51000
	.1181	.3150	.1181	.1496	.3740	.0276	.1575	.1890	.3740	.0354	.006	.150	.283						
93/002	3.00	8.00	-	-	9.50	0.70	3.00	-	9.50	0.70	0.15	3.80	7.20	395	141	Х	-	67000	-
	.1181	.3150			.3740	.0276	.1181		.3740	.0276	.006	.150	.283		100			(7000	
503	3.00	9.00	3.00	-	10.50	0.70	5.00	-	10.50	1.00	0.15	3.80	8.20	571	189	Х	-	67000	-
	.1181	.3543	.1181		.4134	.0276	.1969		.4134	.0394	.006	.150	.323	C 7 1	100	N N		(7000	
603/003	3.00 .1181	9.00 .3543	-	-	-	-	4.00 .1575	-	10.60	0.80	0.20 .008	4.40 .173	7.60 .299	571	189	Х	-	67000	-
03/004			0.50		10.00	0.60			.4173	.0315				571	189	_	_	67000	
03/004	3.00 .1181	9.00 .3543	2.50 .0984	-	10.20 .4016	0.60 .0236	-	-	-	-	0.20 .008	4.40 .173	7.60 .299	571	109	_	_	87000	-
23	3.00	.5545 10.00	4.00	4.80	11.50	1.00	4.00	4.80	11.50	1.00	0.15	4.40	.299 8.60	725	265	Х	V	65000	44000
)23	.1181	.3937	.1575	.1890	.4528	.0394	.1575	.1890	.4528	.0394	.006	.173	.339	725	205	^	^	05000	44000
523/13	3.00	13.00	4.00	4.80	.4520	.0374	4.00	4.80	.4320	.0374	0.15	4.40	8.60	725	265	Х	X	70000	46000
020/10	.1181	.5118	.1575	.1890			.1575	.1890	_		.006	.173	.339	723	200	~	^	70000	40000
533	3.00	13.00	5.00	-	15.00	1.00	5.00	-	15.00	1.00	0.20	4.80	11.20	1339	488	Х		55000	_
	.1181	.5118	.1969		.5906	.0394	.1969		.5906	.0394	.008	.1890	.441	1007	100				
693/0004	3.30	8.00	4.00	-	9.50	0.90	4.00	-	9.50	0.90	0.15	4.10	7.20	625	213	X	<u></u>	80000	-
,	.1299	.3150	.1575	_	.3740	.0354	.1575	_	.3740	.0354	.006	.161	.283						
674/004	4.00	7.00	1.60	-	-	-	1.60	-	-	-	0.08	4.50	6.50	337	129	-	_	60000	-
	.1575	.2756	.0630				.063				.003	.177	.256						
674	4.00	7.00	2.00	-	-	-	2.00	-	-	-	0.08	4.50	6.50	345	130	X	-	67000	-
	.1575	.2756	.0787				.0787				.003	.177	.256			- A		12	Colores .
674/003	4.00	7.00	2.50	-	-	-	2.50	-	8.20	0.60	0.08	4.50	6.50	255	108	Х	-	67000	-
	.1575	.2756	.0984				.0984		.3228	.0236	.003	.177	.256						
93B/0021	4.00	8.00	3.00	-	-	-	3.00	-	-	-	0.15	4.80	7.20	380	127	Х	- / 6	72000	HER
	.1575	.3150	.1181				.1181				.006	.189	.283				123	LIDBOD	
84	4.00	9.00	2.50	3.30	10.30	0.60	4.00	4.80	10.30	1.00	0.10	4.60	8.40	658	226	Х	Х	62000	45000
	.1575	.3543	.0984	.1299	.4055	.0236	.1575	.1890	.4055	.0394	.004	.181	.331						
84/103	4.00	10.00	3.00	-	11.50	0.80	-	-	-	-	0.10	4.60	9.40	658	226	- 4	XIIIX	48000	-
	.1575	.3937	.1181		.4528	.0315					.004	.181	.370	Meet -	1		TTTA		
84/103	4.00	10.00	3.00	-	11.20	0.60	-	-	-	-	0.15	4.80	9.20	711	272	-	-	56000	-
	.1575	.3937	.1181		.4409	.0236					.006	.189	.362						

Note:

(1) f_{s min} = minimum single bearing chamfer or maximum permissible shaft or housing fillet radius
 (2) Other load ratings are possible with different ball complements and non standard retainers
 (3) Different shields and seals are available

⁽⁴⁾ Bearings also available with 1 or 2 shields/seals
 ⁽⁵⁾ Limiting speed also depends on seal, material and the respective ball complement

• Bearings without shields or retainers are also available with recesses.

 Almost all bearing types can also be enhanced with GRW XTRA. Detailed information you can find on page 79 and following. Please discuss your desired design in terms of flange, extended inner ring width, shield, lubrication, and material with our Technical Application Consultants to check availability.





GRW- designation		nensions in 1 m]	Bea	ring without clo	osure in [mm]	[inch]	Bea	aring with clos	ure in [mm] [i	inch]	Chamfer in [mm]		dimensions DIN 5418	Load ratin DIN ISO	gs acc. to	Closure	options ⁽³⁾	Max. limiting sp	beed ⁽⁵⁾ [mm ⁻¹]
accignation	[in	ich]	Width without closure	Width with extended inner ring		imensions t closure	Width with closure	Width with extended inner ring	Flange di with c		[inch]	[n	nm] nch]	0.000	(110)()				
			CIOSUIE	without closure				with closure				Shaft diameter	Housing diameter						
Basic symbol	d	D	В	B ₁	Flange diameter FD	Flange width FB	B ₂	B ₃	Flange diameter FD ₁	Flange width FB ₁	۲ _{s min} (۱)	d _{a min}	D _{a max}	C _r [N]	C _{0r} [N]	Shield ⁽⁴⁾	Seal ⁽⁴⁾	without closure or with shield	with seal
684/10	4.00	10.00	4.00	4.80	11.50	1.00	4.00	4.80	11.50	1.00	0.10	4.60	9.40	711	272	Х	Х	86000	45000
	.1575	.3937	.1575	.1890	.4528	.0394	.1575	.1890	.4528	.0394	.004	.181	.370						
684/10 W8	4.00	10.00	-	-	-	-	4.00	-	11.60	0.80	0.15	4.80	9.20	711	272	Х	-	56000	-
	.1575	.3937					.1575		.4567	.0315	.006	.189	.362						
694	4.00	11.00	4.00	-	12.50	1.00	4.00	-	12.50	1.00	0.15	4.80	10.20	730	271	Х	Х	66000	41000
101	.1575	.4331	.1575		.4921	.0394	.1575		.4921	.0394	.006	.189	.402	704	000	N/	N N	54000	07000
604	4.00 .1575	12.00 .4724	4.00 .1575	-	13.50 .5315	1.00 .0394	4.00 .1575	-	13.50 .5315	1.00 .0394	0.20 .008	5.40 .213	10.60 .417	734	282	Х	X	56000	37000
624	4.00	.4/24 13.00	5.00	5.80	.5315 15.00	1.00	5.00	5.80	15.00	.0394 1.00	0.20	.213 5.80	11.20	1.339	488	Х	~	52000	28000
024	.1575	.5118	.1969	.2283	.5906	.0394	.1969	.2283	.5906	.0394	.008	.228	.441	1.339	400	^	^	52000	28000
694/133	4.00	13.00	5.00	.2203	.3900	.0394	5.00	.2203	.3900	.0394	0.15	4.80	12.20	730	271	Х	X	65000	53000
074/100	.1575	.5118	.1969				.1969		_		.006	.189	.480	/ 50	27 1	~	~	05000	55000
624/16	4.00	16.00	5.00	5.80	-	-	5.00	5.80	-	-	0.20	5.80	12.20	1306	486	Х	X	55000	30000
02.17.10	.1575	.6299	.1969	.2283			.1969	.2283			.008	.228	.480	1000	100			00000	00000
634	4.00	16.00	5.00	-	18.00	1.00	5.00	-	18.00	1.00	0.30	6.40	13.60	1730	670	Х	Х	44000	43000
	.1575	.6299	.1969		.7087	.0394	.1969		.7087	.0394	.012	.252	.535						
624/17	4.00	17.00	5.00	5.80	-	-	5.00	5.80	-	-	0.20	5.80	15.20	1306	486	Х	Х	55000	30000
	.1575	.6693	.1969	.2283			.1969	.2283			.008	.228	.598						
675	5.00	8.00	2.00	-	-	-	2.00	-	-	-	0.08	5.50	7.50	390	160	Х	_	52000	-
	.1969	.3150	.0787				.0787				.003	.217	.295						
675/003	5.00	8.00	2.50	-	9.20	0.60	2.50	-	-	-	0.10	5.60	7.50	218	90	X	- //	63000	-
	.1969	.3150	.0984		.3622	.0236	.0984				.004	.220	.295			1 1200			
675/004	5.00	8.00	3,00	-	-	-	3.00	-	-	-	0.08	5.40	7.60	390	160	Х	-	52000	-
	.1969	.3150	.1181				.1181				.003	.213	.299						
675/094	5.00	9.00	3.00	-	-	-	3.00	-	10.20	0.60	0.15	5.40	8.60	431	169	Х	-	60000	100
	.1969	.3543	.1181				.1181		.4016	.0236	.006	.213	.339			4		di del	A RAN
694A/1002	5.00	10.00	4.00	-	-	-	4.00	-	11.20	0.80	0.15	5.50	8.80	431	169	Х	-	60000	-
(04/1000	.1969	.3937	.1575				.1575		.4409	.0315	.006	.217	.346	700	071	N/			VI. N. C. C.
694/1002	5.00	10.00	4.00	-	-	-	4.00	-	-	-	0.15	5.50	8.80	730	271	Х	- 2	66000	ALLEY
604/1000 \\\1	.1969	.3937	.1575		11.40	0.90	.1575		11.40	0.90	.006	.217	.346	431	140	V	14.211	60000	
694/1002 W1	5.00 .1969	10.00 .3937	4.00 .1575	-	11.60 .4567	0.80 .0315	4.00 .1575	-	11.60 .4567	0.80 .0315	0.15 .006	5.80 .228	9.20 .362	431	169	Х	-	60000	-
685	5.00	.3937 11.00	3.00	_	12.50	0.80	5.00	-	12.50	1.00	0.15	.220 5.80	10.70	734	282	X A		71000	37000
000	.1969	.4331	.1181	-	.4921	.0315	.1969	-	.4921	.0394	.006	.228	.421	/ 54	202		CLAPS	71000	37000
685/003	5.00	11.00	4.00	-	12.50	1.00	4.00	-	12.50	1.00	0.15	5.80	10.70	734	282	Х	- Marine	62000	_
000/000	.1969	.4331	.1575		.4921	.0394	.1575		.4921	.0394	.006	.228	.421	/ 04	202	~		02000	

Note:

(1) f_{s min} = minimum single bearing chamfer or maximum permissible shaft or housing fillet radius
 (2) Other load ratings are possible with different ball complements and non standard retainers
 (3) Different shields and seals are available

⁽⁴⁾ Bearings also available with 1 or 2 shields/seals
 ⁽⁵⁾ Limiting speed also depends on seal, material and the respective ball complement

• Bearings without shields or retainers are also available with recesses.

 Almost all bearing types can also be enhanced with GRW XTRA. Detailed information you can find on page 79 and following. Please discuss your desired design in terms of flange, extended inner ring width, shield, lubrication, and material with our Technical Application Consultants to check availability.





GRW- designation	Main dim [m [ind	m]	Bea Width without closure	ring without clo Width with extended inner ring without closure		mensions		Width with extended inner ring with closure	ure in [mm] [i Flange di with c	imensions	Chamfer in [mm] [inch]	acc. to	g dimensions DIN 5418 [mm] [inch] Housing diameter	Load ratir DIN ISC	igs acc. to) ^[2] (max)	Closure	options ⁽³⁾	Max. limiting sp	beed ⁽⁵⁾ [mm ⁻¹]
Basic symbol	d	D	В	B ₁	Flange diameter FD	Flange width FB	B ₂	B ₃	Flange diameter FD ₁	Flange width FB ₁	r _{s min} (1)	d _{a min}	D _{a max}	C _r [N]	C _{or} [N]	Shield ⁽⁴⁾	Seal ⁽⁴⁾	without closure or with shield	with seal
695	5.00	13.00	4.00	-	15.00	1.00	4.00	-	15.00	1.00	0.20	6.40	11.60	1077	432	Х	Х	50000	34000
	.1969	.5118	.1575		.5906	.0394	.1575		.5906	.0394	.008	.252	.457						
624/0003	5.00	13.00	5.00	-	-	-	5.00	-	15.00	1.00	0.20	6.80	11.20	1306	486	Х	—	52000	-
	.1969	.5118	.1969		1 (00	1.00	.1969		.5906	.0394	.008	.268	.441	1000	507	V	V	50000	22000
505	5.00 .1969	14.00 .5512	5.00 .1969	-	16.00 .6299	1.00 .0394	5.00	-	16.00 .6299	1.00 .0394	0.20 .008	6.40 .252	12.60 .496	1329	507	Х	X	50000	33000
525	5.00	16.00	5.00	5.80	18.00	1.00	5.00	5.80	18.00	1.00	0.30	7.40	13.60	1729	675	Х	V	50000	31000
JZJ	.1969	.6299	.1969	.2283	.7087	.0394	.1969	.2283	.7087	.0394	.012	.291	.535	1729	075	^	^	50000	31000
535	5.00	19.00	6.00	.2200	22.00	1.50	6.00	.2200	22.00	1.50	0.30	7.40	16.60	2522	1.057	Х	X	40000	22000
500	.1969	.7480	.2362		.8661	.0591	.2362		.8661	.0591	.012	.291	.654	2022	1.007	~	~	40000	22000
535/22	5.00	22.00	6.00	6.80	-	-	6.00	6.80	-	-	0.60	7.40	19.60	2458	1.053	Х	Х	43000	25000
,	.1969	.8661	.2362	.2677			.2362	.2677			.024	.291	.772						
76	6.00	10.00	2.50	-	11.20	0.60	-	-	-	-	0.15	6.80	9.20	500	216	_	_	35000	-
	.2362	.3937	.0984		.4409	.0236					.006	.268	.362						
676/003	6.00	10.00	3.00	-	-	-	3.00	-	-	-	0.10	6.60	9.40	503	215	Х	-	46000	-
	.2362	.3937	.1181				.1181				.004	.26	.370						
676/003	6.00	10.00	-	-	-	-	3.00	-	11.20	0.60	0.15	6.80	9.20	500	216	Х	-	35000	-
	.2362	.3937					.1181		.4409	.0236	.006	.268	.362						
695/1232	6.00	12.00	3.00	-	13.20	0.60	-	-	-	-	0.20	7.40	10.60	716	295	-	-	50000	-
	.2362	.4724	.1181		.5197	.0236					.008	.291	.417						
695/1202	6.00	12.00	4.00	-	13.60	0.80	4.00	-	13.60	0.80	0.15	6.80	11.20	851	366	X	Х	49000	28000
	.2362	.4724	.1575		.5354	.0315	.1575		.5354	.0315	.006	.268	.441			[]]]]]]			
686	6.00	13.00	3.50	4.30	15.00	1.00	5.00	5.80	15.00	1.10	0.15	6.80	12.20	1096	437	Х	Х	55000	33000
	.2362	.5118	.1307	.1693	.5906	.0394	.1969	.2283	.5906	.0433	.006	.268	.48	10.10	500				15000
596	6.00	15.00	5.00	-	17.00	1.20	5.00	-	17.00	1.20	0.20	7.40	13.60	1340	523	X	X	46000	45000
40E /0000	.2362	.5906	.1969		.6693	.0472	.1969		.6693	.0472	.008	.291	.535	1444	440	V		41000	KARDEN.
625/0002	6.00 .2362	16.00 .6299	5.00 .1969	-	18.00 .7087	1.00 .0394	5.00 .1969	-	18.00 .7087	1.00 .0394	0.15 .006	8.40 .331	13.60 .535	1646	663	Х	-	41000	-
506	6.00	.0299 17.00	6.00	_	19.00	1.20	6.00	_	19.00	1.20	0.30	8.00	15.00	2263	846	X	v	45000	30000
500	.2362	.6693	.2362	-	.7480	.0472	.2362	_	.7480	.0472	.012	.315	.591	2203	040	~		45000	20000
526	6.00	19.00	6.00	_	22.00	1.50	6.00	_	22.00	1.50	0.30	8.40	16.60	2522	1057	X	X	40000	22000
020	.2362	.7480	.2362		.8661	.0591	.2362		.8661	.0591	.012	.331	.654	LJLL	1007	~	Λ	40000	22000
526/005	6.00	19.00	8.00	_	.0001	.0071	8.00	-	.0001	.0071	0.30	8.40	16.60	2522	1057	x A		48000	_
,	.2362	.7480	.3150				.3150				.012	.331	.654				CHAID	10000	
536	6.00	22.00	7.00	_	-	-	7.00	-	-	-	0.30	8.40	19.60	3333	1423	Х	_	36000	-
	.2362	.8661	.2756				.2756				.012	.331	.772						

Note:

(1) f_{s min} = minimum single bearing chamfer or maximum permissible shaft or housing fillet radius
 (2) Other load ratings are possible with different ball complements and non standard retainers
 (3) Different shields and seals are available

⁽⁴⁾ Bearings also available with 1 or 2 shields/seals
 ⁽⁵⁾ Limiting speed also depends on seal, material and the respective ball complement

• Bearings without shields or retainers are also available with recesses.

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GRVV- designation	[m	nensions in 1 m] 1ch]	Bec Width without closure	rring without clo Width with extended inner ring without	Flange d	[inch] imensions closure		aring with clos Width with extended inner ring with closure	with c	imensions	Chamfer in [mm] [inch]	acc. to [[n [ir Shaft	dimensions DIN 5418 nm] nch] Housing	Load ratin DIN ISO		Closure	options ⁽³⁾	Max. limiting sp	beed ⁽⁵⁾ [mm ⁻¹]
Basic symbol	d	D	В	closure B ₁	Flange diameter FD	Flange width FB	B ₂	B ₃	Flange diameter FD ₁	Flange width FB1	r _{s min} (1)	diameter d _{a min}	diameter D _{a max}	C _r [N]	C _{or} [N]	Shield ⁽⁴⁾	Seal ⁽⁴⁾	without closure or with shield	with seal
677	7.00	11.00	2.50	-	12.20	0.60	-	-	-	-	0.10	7.60	10.40	461	206	_	_	50000	_
	.2756	.4331	.0984		.4803	.0236					.004	.299	.409						
677/003	7.00	11.00	3.00	-	-	-	3.00	-	12.20	0.60	0.10	7.60	10.40	461	206	Х	-	50000	-
	.2756	.4331	.1181				.1181		.4803	.0236	.004	.299	.409						
688A/1322	7.00	13.00	3.00	-	14.20	0.60	4.00	-	14.60	0.80	0.15	8.40	11.60	541	276	Х	Х	48000	30000
	.2756	.5118	.1181		.5591	.0236	.1575		.5748	.0315	.006	.331	.457						
688/1322	7.00	13.00	-	-	-	-	4.00	-	-	-	0.20	8.40	11.60	335	152	Х	-	35000	-
15-201	.2756	.5118					.1575				.008	.331	.457						
687	7.00	14.00	3.50	-	16.00	1.00	5.00	-	16.00	1.10	0.15	7.80	13.20	1186	505	Х	Х	50000	31000
	.2756	.5512	.1307		.6299	.0394	.1969		.6299	.0433	.006	.307	.520	1705					
697	7.00	17.00	5.00	-	19.00	1.20	5.00	-	19.00	1.20	0.30	9.00	15.00	1795	776	Х	Х	39000	28000
407	.2756	.6693	.1969		.7480	.0472	.1969		.7480	.0472	.012	.354	.591	2400	1057	N N	V	42000	00000
607	7.00	19.00	6.00 .2362	-	22.00	1.50	6.00 .2362	-	22.00	1.50	0.30 .012	9.00	17.00 .669	3400	1057	Х	X	43000	22000
627	.2756 7.00	.7480 22.00	.2302 7.00		.8661 25.00	.0591 1.50	.2302 7.00	_	.8661 25.00	.0591 1.50	0.30	.350 9.40	.009 19.60	3369	1363	Х	~	35000	21000
027	.2756	.8661	.2756	-	.9843	.0591	.2756	-	.9843	.0591	.012	.370	.772	5509	1303	^	^	33000	21000
627/28	7.00	28.00	7.00	7.80	.9043	.0391	7.00	7.80	.9043	.0391	0.30	9.40	25.80	3369	1363	Х	_	40000	
027/20	.2756	1.1024	.2756	.3071			.2756	.3071			.012	.370	1.016	3307	1000	~		40000	
678	8.00	12.00	2.50	-	13.20	0.60	.2/00	-	_	-	0.10	8.60	11.40	540	275	_	_	48000	_
0,0	.3150	.4724	.0984		.5197	.0236					.004	.339	.449	010	2,0			10000	
678/003	8.00	12.00	_	-	_	_	3.50	-	13.60	0.80	0.10	8.60	11.40	540	275	X //	<u> </u>	48000	_
	.3150	.4724					.1307		.5354	.0315	.004	.339	.449			1 199			
688A/144	8.00	14.00	3.50	-	15.60	0.80	-	-	-	-	0.15	8.80	13.20	817	386	_	_	45000	-
,	.3150	.5512	.1307		.6142	.0315					.006	.346	.520						
688A/142	8.00	14.00	-	-	-	-	4.00	-	15.60	0.80	0.20	9.40	12.60	817	386	X		47000	
	.3150	.5512					.1575		.6142	.0315	.008	.370	.496			- A		12	
688	8.00	16.00	4.00	-	18.00	1.00	6.00	-	18.00	1.30	0.20	9,40	14.60	1795	776	Х	Х	48000	28000
	.3150	.6299	.1575		.7087	.0394	.2362		.7087	.0512	.008	.370	.575						
688/002	8.00	16.00	-	-	-	-	4.00	-	-	-	0.20	9.40	14.60	1795	776	Х	- / 6	48000	ANTENN
	.3150	.6299					.1575				.008	.370	.575					JUNDO	1 Second
688/003	8.00	16.00	5.00	-	18.00	1.10	5.00	-	18.00	1.10	0.20	9.40	14.60	1795	776	Х	Х	43000	28000
	.3150	.6299	.1969		.7087	.0433	.1969		.7087	.0433	.008	.370	.575						
698	8.00	19.00	6.00	-	22.00	1.50	6.00	-	22.00	1.50	0.30	10.00	17.00	2240	917	X	XXX	43000	27000
	.3150	.7480	.2362		.8661	.0591	.2362		.8661	.0591	.012	.394	.669	NA CONTRACTOR			THIN		
688/20	8.00	20.00	4.00	4.80	-	-	-	-	-	-	0.20	9.40	18.60	1795	776	-	-	45000	-
	.3150	.7874	.1575	.1890							.008	.370	.732						

Note:

(1) f_{s min} = minimum single bearing chamfer or maximum permissible shaft or housing fillet radius
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⁽⁴⁾ Bearings also available with 1 or 2 shields/seals
 ⁽⁵⁾ Limiting speed also depends on seal, material and the respective ball complement

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GRW- designation	Main dim [m [ind	m]	Bear Width without closure	ing without clo Width with extended inner ring without closure		imensions	Bea Width with closure	1	ure in [mm] [in Flange din with cle	mensions	Chamfer in [mm] [inch]	acc. to	g dimensions DIN 5418 mm] inch] Housing diameter		igs acc. to) ^[2] (max)	Closure	options ⁽³⁾	Max. limiting sp	beed ⁽⁵⁾ [mm ⁻¹]
Basic symbol	d	D	В	B ₁	Flange diameter FD	Flange width FB	B ₂	B ₃	Flange diameter FD ₁	Flange width FB ₁	r _{s min} (1)	d _{a min}	D _{a max}	C _r [N]	C _{or} [N]	Shield ⁽⁴⁾	Seal ⁽⁴⁾	without closure or with shield	with seal
508/003	8.00	22.00	6.00	-	-	-	-	-	-	-	0.30	10.00	20.00	3369	1363	-	-	38000	-
	.3150	.8661	.2362								.012	.394	.787						
508	8.00	22.00	7.00	-	25.00	1.50	7.00	-	25.00	1.50	0.30	10.00	20.00	3369	1363	Х	Х	38000	21000
	.3150	.8661	.2756		.9843	.0591	.2756		.9843	.0591	.012	.394	.787						
608/005	8.00	22.00	10.00	-	-	-	10.00	-	-	-	0.30	10.00	20.00	3369	1363	Х	-	43000	-
	.3150	.8661	.3937	-	-	-	.3937	-	-	-	.012	.394	.787						
008/006	8.00	22.00	10.31	-	-	-	10.31	-	-	-	0.30	10.00	20.00	3369	1363	Х	Х	43000	29000
	.3150	.8661	.4059	-	-	-	.4059	-	-	-	.012	.394	.787						
08/007	8.00	22.00	11.00	-	-	-	11.00	-	-	-	0.30	10.00	20.00	3369	1363	Х	Х	43000	29000
	.3150	.8661	.4331				.4331				.012	.394	.787	00/0	1.400	N/	N/	00000	01000
528	8.00	24.00	8.00	-	-	-	8.00	-	-	-	0.30	10.40	21.60	3360	1430	Х	Х	38000	21000
000 (0001	.3150	.9449	.3150				.3150				.012	.409	.850	44.00	1000	N/		25000	
5000/0001	8.00	26.00	8.00	-	-	-	8.00	-	-	-	0.30	10.40	24.00	4698	1982	Х	-	35000	-
400	.3150	1.0236	.3150				.3150				.012	.409	.945	4540	1982	Х		24000	
538	8.00	28.00	9.00	-	-	-	9.00	-	-	-	0.30 .012	10.40 .409	25.60 1.008	4563	1982	X	-	34000	-
679	.3150	1.1024	.3543		15.50	0.90	.3543							919	44.0			12000	
27.4	9.00 .3543	14.00 .5512	3.00 .1181	-	15.50 .6102	0.80 .0315	-	-	-	-	0.10 .004	9.60 .378	13.40 .528		468	-		42000	-
679/003	9.00	14.00	4.50	_	15.50	0.80	4.50	_	15.50	0.80	0.10	9.60	13.40	919	468	Х	v	42000	25000
5/ 9/ 003	.3543	.5512	4.50 .1772	-	.6102	.0315	.1772	-	.6102	.0315	.004	.378	.528	919	400	^	^	42000	23000
589	9.00	17.00	4.00	4.80	19.00	1.00	6.00	_	19.00	1.30	0.20	10.40	15.60	1798	797	X	X	44000	27000
009	.3543	.6693	.1575	.1890	.7480	.0394	.2362	_	.7480	.0512	.008	.409	.614	17 90	/ 7/		^	44000	27000
589/003	9.00	17.00	5.00	.1070	.7400	.0374	5.00	-	.7400	.0312	0.20	10.40	15.60	1798	797	X	_	44000	_
507/005	.3543	.6693	.1969	_		_	.1969			_	.008	.409	.614	17 90	/ 7/	~		44000	
599	9.00	20.00	6.00	6.80	23.00	1.50	6.00	6.80	23.00	1.50	0.30	11.00	18.00	2467	1081	X	X	40000	25000
	.3543	.7874	.2362	.2677	.9055	.0591	.2362	.2677	.9055	.0591	.012	.433	.709	2407	1001	, A L	~	40000	20000
509	9.00	24.00	7.00	-	27.00	1.50	7.00	-	27.00	1.50	0.30	11.00	22.00	3435	1430	Х	Х	33000	20000
	.3543	.9449	.2756		1.0630	.0591	.2756		1.0630	.0591	.012	.433	.866	0.000				00000	20000
529	9.00	26.00	8.00	8.80	28.00	2.00	8.00	8.80	28.00	2.00	0.30	11.40	23.60	4.698	1982	Х	X	34000	19000
·	.3543	1.0236	.3150	.3465	1.1024	.0787	.3150	.3465	1.1024	.0787	.012	.449	.929				1/1/2	171AX	Andrew
6700	10.00	15.00	3.00	-	16.50	0.80	-	-	16.50	0.80	0.15	10.80	14.20	855	435	-	-	17000	-
	.3937	.5906	.1181		.6496	.0315			.6496	.0315	.006	.425	.559						
5700/003	10.00	15.00	4.00	-	16.50	0.80	4.00	-	16.50	0.80	0.15	10.80	14.20	855	435	x A	KA XIXO	17000	10000
,	.3937	.5906	.1575		.6496	.0315	.1575		.6496	.0315	.006	.425	.559			AL AL	and a		
6800 (4)	10.00	19.00	5.00	5.80	21.00	1.00	7.00	7.80	21.00	1.50	0.30	12.00	17.00	1922	915	Х	Х	42000	25000
, ,	.3937	.7480	.1969	.2283	.8268	.0394	.2756	.3071	.8268	.0591	.012	.472	.669						

Note:

(1) f_{s min} = minimum single bearing chamfer or maximum permissible shaft or housing fillet radius
 (2) Other load ratings are possible with different ball complements and non standard retainers
 (3) Different shields and seals are available

⁽⁴⁾ Bearings also available with 1 or 2 shields/seals
 ⁽⁵⁾ Limiting speed also depends on seal, material and the respective ball complement

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GRW- designation	Main dim [m	ensions in ml	Bea	ring without clo	sure in [mm] [[inch]	Bec	aring with closu	ure in [mm] [inch]	Chamfer in [mm]		dimensions NN 5418	Load ratir DIN ISC	igs acc. to ⁽²⁾ (max)	Closure	options ⁽³⁾	Max. limiting sp	peed ⁽⁵⁾ [mm ⁻¹]
	[in-	ch]	Width without closure	Width with extended inner ring without	Flange di without	imensions closure	Width with closure	Width with extended inner ring with closure		imensions closure	[inch]	[ir Shaft	hm] hch] Housing		,				
				closure		I.				1		diameter	diameter		1		1		1
Basic symbol	d	D	В	B ₁	Flange diameter FD	Flange width FB	B ₂	B ₃	Flange diameter FD ₁	Flange width FB ₁	r _{s min} (1)	d _{a min}	D _{a max}	C _r [N]	C _{Or} [N]	Shield ⁽⁴⁾	Seal ⁽⁴⁾	without closure or with shield	with seal
6800/002	10.00	19.00	-	-	-	-	5.00	-	21.00	1.00	0.30	12.00	17.00	1922	915	Х	-	34000	-
	.3937	.7480					.1969		.8268	.0394	.012	.472	.669						
800/003	10.00	19.00	6.00	-	-	-	6.00	-	-	-	0.30	12.00	17.00	1922	915	Х	-	35000	-
200/202	.3937	.7480	.2362				.2362				.012	.472	.669	1922	915	Х		34000	
800/202	10.00 .3937	20.00 .7874	-	-	-	-	5.00 .1969	-	-	-	0.30 .012	12.00 .472	18.00 .709	1922	91 <u>3</u>	A	-	34000	_
900	10.00	22.00	6.00	_	25.00	1.50	6.00	-	25.00	1.50	0.30	12.00	20.00	2695	1273	Х	Х	41000	24000
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	.3937	.8661	.2362		.9843	.0591	.2362		.9843	.0591	.012	.472	.787	2073	1270	~	~	41000	24000
000	10.00	26.00	8.00	8.80	28.00	2.00	8.00	8.80	28.00	2.00	0.30	12.40	23.60	4698	1982	Х	Х	35000	19000
	.3937	1.0236	.3150	.3465	1.1024	.0787	.3150	.3465	1.1024	.0787	.012	.488	.929						
000/003	10.00	26.00	10.00	-	-	-	10.00	-	-	-	0.30	12.40	23.60	4149	1388	Х	-	38000	-
	.3937	1.0236	.3937				.3937				.012	.488	.929						
6100	10.00	28.00	8.00	-	-	-	8.00	-	-	-	0.30	14.20	23.80	4620	1960	Х	_	37000	-
	.3937	1.1024	.3150				.3150				.012	.559	.937						
5200	10.00	30.00	9.00	-	-	-	9.00	-	-	-	0.60	14.20	25.80	4340	1920	Х	Х	27000	18000
	.3937	1.1811	.3543				.3543				.024	.559	1.016						
300	10.00	35.00	11.00	-	-	-	11.00	-	-	-	0.60	14.20	20.80	6870	2750	Х	Х	27000	18000
	.3937	1.3780	.4331				.4331				.024	.559	.819						
701	12.00	18.00	4.00	-	19.50	0.80	4.00	-	19.50	0.80	0.20	13.40	16.60	926	530	Х	Х	15000	10000
	.4724	.7087	.1575		.7677	.0315	.1575		.7677	.0315	.008	.528	.654						
801	12.00	21.00	5.00	-	-	-	5.00	-	-	-	0.30	14.00	19.00	1930	900	X		30000	
	.4724	.8268	.1969				.1969				.012	.551	.748						
801/003	12.00	21.00	6.00	-	-	-	6.00	-	-	-	0.30	14.00	19.00	1720	840	Х	-	32000	-
001/004	.4724	.8268	.2362		00.00	1.50	.2362		00.00	1.50	.012	.551	.748	1015	1041	V	V	20000	24000
801/004	12.00 .4724	21.00 .8268	7.00 .2756	-	23.00 .9055	1.50 .0591	7.00 .2756	-	23.00 .9055	1.50 .0591	0.30 .012	14.00 .551	19.00 .748	1915	1041	X	X	39000	24000
5901	12.00	24.00	6.00	_	.9033	.0391	6.00	_	.9033	.0391	0.30	14.00	22.00	2971	1460	X	_	32000	<u></u>
J901	.4724	.9449	.2362	_	-	_	.2362		-	-	.012	.551	.866	2971	1400	~		32000	
6001	12.00	28.00	7.00	_	-	-	7.00	-	_	-	0.30	14.00	26.00	5100	2370		- //Z)	32000	ALLE
0001	.4724	1.1024	.2756				.2756				.012	.551	1.024	5100	2010		112		also
001	12.00	28.00	8.00	_	30.00	2.00	8.00	-	30.00	2.00	0.30	14.00	26.00	5237	2370	Х	X	31000	17000
	.4724	1.1024	.3150		1.1811	.0787	.3150		1.1811	.0787	.012	.551	1.024	0207	20/0		~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	0.000	17 000
001/003	12.00	28.00	11.00	-	-	-	11.00	-	-	-	0.30	14.00	26.00	5237	2359	X A	BKL FT BKC	31000	_
,	.4724	1.1024	.4331				.4331				.012	.551	1.024	n			ALLA		
3001	12.00	28.00	12.00	-	-	-	12.00	-	-	-	0.50	14.00	26.00	5100	2370	Х	Х	30000	16000
	.4724	1.1024	.4724				.4724				.020	.551	1.024						

Note:

(1) f_{s min} = minimum single bearing chamfer or maximum permissible shaft or housing fillet radius
 (2) Other load ratings are possible with different ball complements and non standard retainers
 (3) Different shields and seals are available

⁽⁴⁾ Bearings also available with 1 or 2 shields/seals
 ⁽⁵⁾ Limiting speed also depends on seal, material and the respective ball complement

• Bearings without shields or retainers are also available with recesses.

 Almost all bearing types can also be enhanced with GRW XTRA. Detailed information you can find on page 79 and following. Please discuss your desired design in terms of flange, extended inner ring width, shield, lubrication, and material with our Technical Application Consultants to check availability.





GRW- designation	Main dime [m [inc	ensions in m] ch]	Bea Width without closure	ring without clo Width with extended inner ring without closure	sure in [mm] [Flange di without	mensions	Bea Width with closure	Width with extended inner ring with closure	Flange d	inch] imensions closure	Chamfer in [mm] [inch]	acc. to [[n	dimensions DIN 5418 1 m] Ich] Housing diameter	Load ratin DIN ISC	igs acc. to) ^[2] (max)	Closure	options ⁽³⁾	Max. limiting sp	beed ⁽⁵⁾ [mm ⁻¹]
Basic symbol	d	D	В	B ₁	Flange diameter FD	Flange width FB	B ₂	B ₃	Flange diameter FD ₁	Flange width FB ₁	r _{s min} ⁽¹⁾	d _{a min}	D _{a max}	C _r [N]	C _{Or} [N]	Shield ⁽⁴⁾	Seal ⁽⁴⁾	without closure or with shield	with seal
16101	12.00	30.00	8.00	-	-	-	8.00	-	-	-	0.50	14.40	27.60	5070	2360	Х	Х	28000	16000
(001	.4724	1.1811	.3150				.3150				.020	.567	1.087	5770	0.450	V	V	0/000	1,5000
5201	12.00 .4724	32.00 1.2598	10.00 .3937	-	-	-	10.00 .3937	-	-	-	0.60 .024	16.20 .638	27.80 1.094	5770	2450	Х	Х	26000	15000
52201	12.00	32.00	.3937 14.00	_	-	-	.3937 14.00	_	_	_	0.60	16,20	27.80	6890	3100	Х	Х	25000	15000
	.4724	1.2598	.5512				.5512				.024	.638	1.094	0070	0100	~	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	20000	10000
5301	12.00	37.00	12.00	-	-	-	12.00	-	-	-	1.00	17.60	31.40	8240	3360	Х	Х	25000	14000
	.4724	1.4567	.4724				.4724				.039	.693	1.236						
52301	12.00	37.00	17.00	-	-	-	17.00	-	-	-	1.00	17,60	31.40	8240	3360	-	Х	27000	14000
	.4724	1.4567	.6693				.6693				.039	.693	1.236						
6702	15.00	21.00	4.00	-	-	-	4.00	-	-	-	0.20	16.40	19.60	937	582	Х	Х	13000	9000
	.5906	.8268	.1575				.1575				.008	.646	.772						
802	15.00	24.00	5.00	-	-	-	5.00	-	-	-	0.30	17.00	22.00	2080	1100	Х	Х	25000	15000
/	.5906	.9449	.1969				.1969				.012	.669	.866						
5802/003	15.00	24.00	7.00	-	26.00	1.50	7.00	-	26.00	1.50	0.30	17.00	22.00	2073	1253	Х	Х	33000	18000
4000	.5906 15.00	.9449 28.00	.2756 7.00	—	1.0236	.0591	.2756 7.00	-	1.0236	.0591	.012	.669 17.00	.866 26.00	4445	2268	V	X	24000	16000
5902	.5906	28.00 1.1024	.2756	-	-	-	.2756	-	-	-	0.30 .012	.669	1.024	4445	2208	Х	~	24000	10000
16002	15.00	32.00	.2730 8.	_	-	_	8.00	_	_	_	0.50	17.00	30.00	5600	2830	Х	X	26000	14000
10002	.5906	1.2598	.3150	_	_	_	.3150		_		.020	.669	1.181	5000	2000	Λ.	~	20000	14000
5002	15.00	32.00	9.00	_	-	-	9.00	-	_	-	0.30	17.00	30.00	5676	2819	X //		25000	_
	.5906	1.2598	.3543				.3543				.012	.669	1.181		2017			20000	
5202	15.00	35.00	11.00	-	-	-	11.00	-	-	-	0.60	19.20	30.80	6490	3000	Х	Х	24000	16000
	.5906	1.3780	.4331				.4331				.024	.756	1.213						
52202	15.00	35.00	14.00	-	-	-	14.00	-	-	-	0.60	19.20	30.80	7650	3750	X	Х	23000	13000
	.5906	1.3780	.5512				.5512				.024	.756	1.213		1 200			all and	
5302	15.00	42.00	13.00	-	-	-	13.00	-	-	-	1.50	24.00	33.00	11400	5450	Х	Х	21000	11000
	.5906	1.6535	.5118				.5118				.059	.945	1.299	June 1997					N/1 W /3-1-1
703	17.00	23.00	4.00	-	24.50	0.80	4.00	-	24.50	0.80	0.20	18.40	21.60	1000	658	Х	X	11000	7000
	.6693	.9055	.1575		.9646	.0315	.1575		.9646	.0315	.008	.724	.850	1/12			Product	LINKO	
5803	17.00	26.00	5.00	-	-	-	5.00	-	-	-	0.30	19.00	24.00	2240	1270	Х	-	22000	-
000	.6693	1.0236	.1969				.1969				.012	.748	.945	1700	0547	× 4		01000	
903	17.00 .6693	30.00 1.1811	7.00 .2756	-	-	-	7.00 .2756	-	-	-	0.30 .012	1.00 .748	28.00 1.102	4723	2547	X	CIF19	21000	-
6003	.0093 17.00	35.00	.2/50 8.00	_	_	-	.2/30 8.00	-	_	_	0.30	./48 19.00	33.00	6000	3250	X	260742	23500	_
0005	17.00	35.00 1.378	.3150	-	_	-	.3150		_	_	.012	.748	1.299	0000	5250	^		23300	_

Note:

(1) f_{s min} = minimum single bearing chamfer or maximum permissible shaft or housing fillet radius
 (2) Other load ratings are possible with different ball complements and non standard retainers
 (3) Different shields and seals are available

⁽⁴⁾ Bearings also available with 1 or 2 shields/seals
 ⁽⁵⁾ Limiting speed also depends on seal, material and the respective ball complement

• Bearings without shields or retainers are also available with recesses.

 Almost all bearing types can also be enhanced with GRW XTRA. Detailed information you can find on page 79 and following. Please discuss your desired design in terms of flange, extended inner ring width, shield, lubrication, and material with our Technical Application Consultants to check availability.





GRW- designation	Main dim [m [in		Width	ring without clo Width with	Flange di	imensions	Width with	Width with	ure in [mm] [ir Flange dir	mensions	Chamfer in [mm] [inch]	acc. to I	dimensions DIN 5418 nm]	Load ratir DIN ISC	ngs acc. to) ⁽²⁾ (max)	Closure	options ⁽³⁾	Max. limiting sp	peed ⁽⁵⁾ [mm ⁻¹]
			without closure	extended inner ring without closure	without	closure	closure	extended inner ring with closure	with cl	osure		Lii Shaft diameter	nch] Housing diameter						
Basic symbol	d	D	В	B ₁	Flange diameter FD	Flange width FB	B ₂	B ₃	Flange diameter FD ₁	Flange width FB ₁	[s min (1)	d _{a min}	D _{a max}	C _r [N]	C _{0r} [N]	Shield ⁽⁴⁾	Seal ⁽⁴⁾	without closure or with shield	with seal
6003	17.00	35.00	10.00	-	-	-	10.00	-	-	-	0.30	19.00	33.00	5090	2630	Х	Х	23000	18000
	.6693	1.3780	.3937				.3937				.012	.748	1.299						
6203	17.00	40.00	12.00	-	-	-	12.00	-	-	-	0.60	21.20	35.80	8130	3850	Х	Х	20000	15000
0000	.6693	1.5748	.4724				.4724				.024	.835	1.409	05/0	4750	N N		01000	
62203	17.00 .6693	40.00 1.5748	16.00 .6299	-	-	-	16.00 .6299	-	-	-	0.60 .024	21.20 .835	35.80 1.409	9560	4750	Х	-	21000	-
303	1 7.00	47.00	1 4.00	_	-	_	14.00	_	_	_	1.00	22.60	41.40	11550	5330	Х	X	18000	14000
0000	.6693	1.8504	.5512	_	-	_	.5512		_	_	.039	.890	1.630	11550	5550	^	^	18000	14000
6704	20.00	27.00	4.00	_	28.50	0.80	4.00	-	28.50	0.80	0.20	22.00	25.60	1402	729	Х	X	10000	7000
	.7874	1.0630	.1575		1.122	.0315	.1575		1.122	.0315	.008	.866	1.008	1102	, , ,	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		10000	, 000
6804	20.00	32.00	7.00	-	35.00	1.50	7.00	-	35.00	1.50	0.30	22.00	30.00	4015	2462	Х	Х	25000	13000
	.7874	1.2598	.2756		1.378	.0591	.2756		1.378	.0591	.012	.866	1.181						
904	20.00	37.00	9.00	-	40.00	2.00	9.00	2.00	40.00	2.00	0.30	22.00	35.00	6381	3682	Х	Х	23000	12000
	.7874	1.4567	.3543		1.5748	.0787	.3543	.0787	1.5748	.0787	.012	.866	1.378						
16004	20.00	42.00	8.00				8.00				0.30	22.00	40.00	6940	4100	Х	-	21000	-
	.7874	1.6535	.3150				.3150				.012	.866	1.575						
6004	20.00	42.00	12.00	-	-	-	12.00	-	-	-	1.00	24.60	37.40	7900	4250	Х	Х	21000	11000
	.7874	1.6535	.4724				.4724				.039	.969	1.472						
6204	20.00	47.00	14.00	-	-	-	14.00	-	-	-	1.00	25.60	41.40	10910	5360	Х	Х	17000	10000
	.7874	1.8504	.5512				.5512				.039	1.008	1.630						
6705	25.00	32.00	4.00	-	-	-	4.00	-	34.00	1.00	0.20	27.00	30.60	1091	838	/-///	Х	12000	8000
	.9843	1.2598	.1575				.1575		1.3386	.0394	.008	1.063	1.205			//////			di di Alena
6805	25.00	37.00	7.00	-	40.00	1.50	7.00	-	40.00	1.50	0.30	27.00	35.00	4303	2932	X	-	21000	-
1005	.9843	1.4567	.2756		1.5748	.0591	.2756		1.5748	.0591	.012	1.063	1.378	7001	1510	N	N N	10000	10000
6905	25.00 .9843	42.00	9.00 .3543	-	45.00 1.7717	2.00 .0787	9.00	-	45.00 1.7717	2.00 .0787	0.30 .012	27.00	40.00 1.575	7001	4540	X	X	19000	10000
16005	.9843 25.00	1.6535 47.00	.3543 8.00	_		.0787	.3543 8.00		1.//1/	.0787	0.60	1.063	_	8550	4690	X	_	17000	
10005	.9843	47.00 1.8504	.3150	-	-	-	.3150	-	-	-	.024	27.00 1.063	45.00 1.772	8550	4090	^	_	17000	_
5005	25.00	47.00	12.00	_	-	_	12.00	_	_	-	0.60	28.20	43.80	8550	4690	Х	X	18000	9500
5005	.9843	1.8504	.4724	-		_	.4724		-	-	.024	1.110	1.724	0000	4070	~		H BOOK	213000
5706	30.00	37.00	4.00	-	39.00	1.00	4.00	-	39.00	1.00	0.20	32.00	35.60	1143	947	Х	_	17000	_
0,00	1.1811	1.4567	.1575		1.5354	.0394	.1575		1.5354	.0394	.008	1.260	1.402	1140	/-+/	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		17000	
5806	30.00	42.00	7.00	-	45.00	1.50	7.00	-	45.00	1.50	0.30	32.00	40.00	4538	3402	X A		18000	9000
	1.1811	1.6535	.2756		1.7717	.0591	.2756		1.7717	.0591	.012	1.260	1.575				ATTA		,000
6906	30.00	47.00	9.00	-	50.00	2.00	9.00	-	50.00	2.00	0.30	32.00	45.00	7242	5003	Х	Х	17000	8500
	1.1811	1.8504	.3543		1.9685	.0787	.3543		1.9685	.0787	.012	1.260	1.772						

Note:

(1) f_{s min} = minimum single bearing chamfer or maximum permissible shaft or housing fillet radius
 (2) Other load ratings are possible with different ball complements and non standard retainers
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⁽⁴⁾ Bearings also available with 1 or 2 shields/seals
 ⁽⁵⁾ Limiting speed also depends on seal, material and the respective ball complement

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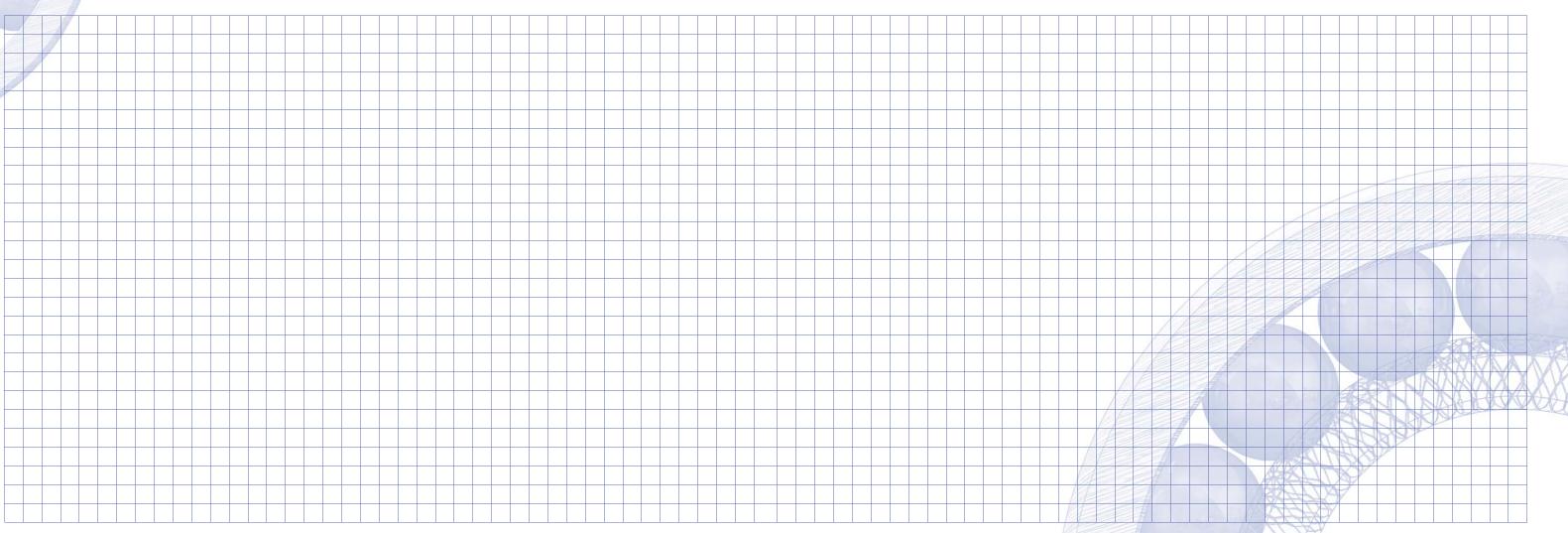
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	GRW- designation	[m	nensions in I m] .ch]	Bec Width without closure	ring without clo Width with extended inner ring without closure		imensions		rring with closu Width with extended inner ring with closure	ure in [mm] [i Flange di with c	mensions	Chamfer in [mm] [inch]	acc. to	i dimensions DIN 5418 nm] nch] Housing diameter		gs acc. to ⁽²⁾ (max)	Closure (options ⁽³⁾	Max. limiting spe	eed ⁽⁵⁾ [mm ⁻¹]
NNN NNN	Basic symbol	d	D	В	B ₁	Flange diameter FD	Flange width FB	B ₂	B ₃	Flange diameter FD ₁	Flange width FB ₁	r _{s min} (1)	d _{a min}	D _{a max}	C _r [N]	C _{0r} [N]	Shield ⁽⁴⁾	Seal ⁽⁴⁾	without closure or with shield	with seal
	6807	35.00 1.3780	47.00 1.8504	7.00 .2756	-	50.00 1.9685	1.50 .0591	7.00 .2756	-	50.00 1.9685	1.50 .0591	0.30 .012	37.00 1.457	45.00 1.772	4729	3821	Х	Х	16000	8000

Your Notes:



Note:

 $^{(1)}$ r_{s min} = minimum single bearing chamfer or maximum permissible shaft or housing fillet radius $^{(2)}$ Other load ratings are possible with different ball complements and non standard retainers ⁽³⁾ Different shields and seals are available

⁽⁴⁾ Bearings also available with 1 or 2 shields/seals ⁽⁵⁾ Limiting speed also depends on seal, material and the respective ball complement

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• Subject to change.

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GRW designation	[r	nensions in nm] 1ch]	Wldth without	ing without clos Width with extended	Flange d	nch] imensions closure		aring with clos Width with extended	Flange d	nch] limensions closure	Chamfer in [mm] [inch]	to ANSI/AFI	dimensions acc. BMA Std. 12.2 in [mm] inch]	Load ratin DIN ISC	gs acc. to) ^[2] (max)	Closure	options ⁽³⁾	Max. limiting s	peed ⁽⁵⁾ [mm ⁻¹]
			closure	inner ring without closure				inner ring with closure				Shaft diameter	Housing diameter						
Basic symbol	d	D	В	B ₁	Flange diameter FD	Flange width FB	B ₂	B ₃	Flange diameter FD ₁	Flange width FB ₁	۲ _{s min} (1)	d _{a min}	D _{a max}	C [N]	C _{or} [N]	Shield ⁽⁴⁾	Seal ⁽⁴⁾	without closure or with shield	with seal
016	1.016	3.175	1.191	-	-	-	-	-	-	-	0.08	1.50	2.65	106	28	-	-	150000	_
	.0400	.1250	.0469								.003	.059	.104						
191	1.191	3.967	1.588	2.381	5.156	0.330	-	-	-	-	0.08	1.80	3.35	163	44	-	-	129000	-
	.0469	.1562	.0625	.0937	.2030	.0130					.003	.071	.132						
397	1.397	4.763	1.984	-	-	-	2.779	-	5.944	0.787	0.08	2.00	4.15	239	67	Х	-	114000	-
	.0550	.1875	.0781				.1094		.2340	.03100	.003	.079	.163						
/64	1.984	6.350	2.380	3.175	7.518	0.584	3.571	4.366	7.518	0.787	0.08	2.60	5.75	286	90	Х	-	95000	-
	.0781	.2500	.0937	.1250	.2960	.0230	.1406	.1719	.2960	.0310	.003	.102	.226	100				0.4000	
380	2.380	4.763	1.588	2.380	5.944	0.457	2.380	3.175	5.944	0.787	0.08	2.90	4.25	192	59	Х	_	94000	-
175 (0000	.0937	.1875	.0625	.0937	.2340	.0180	.0937	.1250	.2340	.0310 0.787	.003	.114 2.95	.167	292	97	V		00000	
75/0002	2.380	6.350 .2500	2.779 .1094	-	7.518	0.787	2.779 .1094	-	7.518 .2960		0.08 .003		5.75	292	97	Х	_	82000	-
′32	.0937 2.380	7.938	2.779	3.571	.2960 9.119	.0310 0.584	3.571	4.366	9.119	.0310 0.787	0.08	.116 3.10	.226 7.25	644	215	X	X	62000	5100
JZ	.0937	.3125	.1094	.1406	.3590	.0230	.1406	4.300 .1719	.3590	.0310	.003	.122	·23	044	213	^	^	02000	5100
75/002	3.175	6 .350			.3590	.0230	2.380	.1719	7.518	0.584	0.08	3.75	5.75	311	109	X	_	80000	_
17 37 002	.1250	.2500	_	_	_	_	.0937	_	.2960	.0230	.003	.148	.226	511	109	^	_	80000	_
175	3.175	6.350	2.380	3.175	7.518	0.584	2.779	3.571	7.518	0.787	0.08	3.75	5.75	292	97	X	X	80000	5300
/5	.1250	.2500	.0937	.1250	.2960	.0230	.1094	.1406	.2960	.0310	.003	.148	.226	272	77	~	~	00000	5500
175A	3.175	6.350	2.380		7.518	0.584	2.779	-	7.518	0.787	0.08	3.75	5.75	311	109	X		80000	
	.1250	.2500	.0937		.2960	.0230	.1094		.2960	.0310	.003	.148	.226	011	107			00000	
/8A	3.175	7.938	2.779	3.571	9.119	0.584	3.571	4.366	9.119	0.787	0.08	3.90	7.20	644	215	X	X	65000	5100
	.1250	.3125	.1094	.1406	.3590	.0230	.1406	.1719	.3590	.0310	.003	.154	.283						
175/061	3.175	9.525	2.779	-	-	-	2.779	-	-	-	0.08	3.90	8.80	292	97	X	_	80000	-
	.1250	.3750	.1094				.1094				.003	.154	.346						
175/6	3.175	9.525	-	-	-	_	2.779	-	-	-	0.08	3.90	8.80	292	/97	X	-	80000	-
	.1250	.3750					.1094				.003	.154	.346			E.		12	ALCON.
/8A/6	3.175	9.525	-	-	-	-	3.571	4.366	10.719	0.787	0.08	3.90	8.80	644	215	Х	Х	82000	5100
	.1250	.3750					.1406	.1719	.4220	.0310	.003	.154	.346						
/8B	3.175	9.525	3.967	4.763	11.176	0.762	3.967	4.763	11.176	0.762	0.30	4.55	8.25	720	260	Х	X	61000	4400
	.1250	.3750	.1562	.1875	.4400	.0300	.1562	.1875	.4400	.0300	.012	.179	.325				1.08	MAR P	Sec.
75/552	3.175	10.414	-	-	-	-	2.380	-	-	-	0.08	3.75	8.40	292	97	Х	-	80000	-
	.1250	.4100					.0937				.003	.148	.331						
75/8	3.175	12.700	-	-	-	-	2.779	3.571	-	-	0.08	4.55	11.35	292	97	X	XT-TX	80000	-
	.1250	.5000					.1094	.1406			.003	.179	.447	M		N2	SHUR		
/8B/083	3.175	12.700	4.366	-	-	-	4.366	-	-	-	0.30	4.55	11.35	725	265	Х	-	74000	-
	.1250	.5000	.1719				.1719				.012	.179	.447						

Note:

(1) f_{s min} = minimum single bearing chamfer or maximum permissible shaft or housing fillet radius
 (2) Other load ratings are possible with different ball complements and non standard retainers
 (3) Different shields and seals are available

⁽⁴⁾ Bearings also available with 1 or 2 shields/seals
 ⁽⁵⁾ Limiting speed also depends on seal, material and the respective ball complement

• Bearings without shields or retainers are also available with recesses.

 Almost all bearing types can also be enhanced with GRW XTRA. Detailed information you can find on page 79 and following. Please discuss your desired design in terms of flange, extended inner ring width, shield, lubrication, and material with our Technical Application Consultants to check availability.





GRW designation	[r	nensions in nm] Ich]	Wldth	ing without clos Width with	Flange d	imensions	Width with	aring with clos Width with	Flange d	imensions	Chamfer in [mm] [inch]	to ANSI/AFE	dimensions acc. BMA Std. 12.2 in [mm]	Load ratin DIN ISO		Closure	options ⁽³⁾	Max. limiting s	peed ⁽⁵⁾ [mm ⁻¹]
			without closure	extended inner ring without closure	without	closure	closure	extended inner ring with closure	with o	closure		Shaft diameter	inch] Housing diameter						
Basic symbol	d	D	В	B ₁	Flange diameter FD	Flange width FB	B ₂	B ₃	Flange diameter FD ₁	Flange width FB ₁	۲ _{s min} (1)	d _{a min}	D _{a max}	С [Ń]	C _{or} [N]	Shield ⁽⁴⁾	Seal ⁽⁴⁾	without closure or with shield	with seal
3967/002	3.967	7.938	-	-	_	-	2.779	-	-	-	0.08	4.55	7.30	391	165	Х	-	65000	-
	.1562	.3125					.1094				.003	.179	.287						
3967	3.967	7.938	2.779	3.571	9.119	0.584	3.175	3.967	9.119	0.914	0.08	4.55	7.30	391	165	Х	Х	68000	42000
	.1562	.3125	.1094	.1406	.3590	.0230	.1250	.1562	.3590	.0360	.003	.179	.287						
4763A/002	4.763	7.938	-	-	-	-	2.779	-	-	-	0.08	5.35	7.30	391	165	Х	-	61000	-
	.1875	.3125					.1094				.003	.211	.287						
4763A	4.763	7.938	2.779	3.571	9.119	0.584	3.175	3.967	9.119	0.914	0.08	5.35	7.30	391	165	Х	Х	65000	42000
17101/1010	.1875	.3125	.1094	.1406	.3590	.0230	.1250	.1562	.3590	.0360	.003	.211	.287		1.4.5			/ 5000	(0000
4763A/062	4.763	9.525	2.779	-	-	-	2.779	-	-	—	0.08	5.35	7.30	391	165	Х	Х	65000	42000
474.00	.1875	.3750	.1094	0.0/7	10 710	0.504	.1094	0.07	10 710	0.707	.003	.211	.287	700	071	V	V	54000	41000
4763B	4.763	9.525	3.175	3.967	10.719	0.584	3.175	3.967	10.719	0.787	0.08 .003	5.50	8.80	730	271	Х	X	56000	41000
4763A/082	.1875 4.763	.3750 12.700	.1250	.1562	.4220	.0230	.1250 2.779	.1562 3.571	.4220	.0310	0.08	.217 5.35	.346 8.80	391	165	V		70000	
4703A7062	4.703 .1875	.5000	_	_	_	_	.1094	.1406	_	_	.003		346	241	105	Х	-	/0000	-
4763B/083	4.763	12.700	3.967	_	_	_	3.967	.1400	_	_	0.08	6.20	11.35	730	271	Х	_	56000	_
4/030/003	.1875	.5000	.1562				.1562				.003	.244	.447	/ 50	27 1	^		30000	
3/16/002	4.763	12.700	.1502	_	_	_	3.967	_	_	_	0.30	6.20	11.35	1339	488	Х	_	50000	
37 107 002	.1875	.5000					.1562				.012	.244	.447	1007	400	~		30000	
3/16	4.763	12.700	3.967	4.763	14.351	1.067	4.978	5.771	14.351	1.067	0.30	6.20	11.35	1339	488	Х	X	50000	37000
0/10	.1875	.5000	.1562	.1875	.5000	.0420	.1960	.2272	.5000	.0420	.012	.244	.447	1007	400	~	~	30000	0,000
4763B/084	4.763	12.700	2.779				5.558				0.30	6.20	11.35	730	271			43000	_
., 000, 001	.1875	.5000	.1094				.2188				.012	.244	.447	,		1 11/2			
1/4A/0001	4.763	15.875	4.978	_	17.526	1.067	4.978	_	17.526	1.067	0.30	6.20	14.35	1651	670	Х	Х	41000	31000
	.1875	.6250	.1960		.6900	.0420	.196		.6900	.0420	.012	.244	.565						
6350A	6.350	9.525	3.175	3.967	10.719	0.584	3.175	3.967	10.719	0.914	0.08	6.90	8.95	391	165	X	X	54000	35000
	.2500	.3750	.1250	.1562	.4220	.02300	.1250	.1562	.4220	.0360	.003	.272	.352			E.		12	AN AND
6350B	6.350	12.700	3.175	3.967	13.894	0.584	4.763	5.558	13.894	1.143	0.13	7.20	11.85	730	271	Х	Х	38000	33000
	.2500	.5000	.1250	.1562	.5000	.02300	.1875	.2188	.5000	.0450	.005	.283	.467						
1/4A	6.350	15.875	4.978	5.771	17.526	1.067	4.978	5.771	17.526	1.067	0.30	7.85	14.35	1651	670	Х	X	43000	31000
	.2500	.6250	.1960	.2272	.6900	.0420	.1960	.2272	.6900	.0420	.012	.309	.565				1/284	LIDRR	Sec.
1/4/002	6.350	19.050	-	-	-	-	5.558	-	-	-	0.41	8.20	17.20	2522	1057	Х	Х	35000	28000
	.2500	.7500					.2188				.016	.323	.677						
1/4	6.350	19.050	5.558	-	-	-	7.142	-	-	-	0.41	8.20	17.20	2522	1057	X	XXX	35000	28000
	.2500	.7500	.2188				.2812				.016	.323	.677	VA CO		/2	STITZ		
7938	7.938	12.700	3.967	4.763	13.894	0.787	3.967	4.763	13.894	0.787	0.13	8.80	11.85	539	279	Х	Х	45000	30000
	.3125	.5000	.1562	.1875	.5000	.03100	.1562	.1875	.5000	.0310	.005	.346	.467				A AV		

Note:

(1) f_{s min} = minimum single bearing chamfer or maximum permissible shaft or housing fillet radius
 (2) Other load ratings are possible with different ball complements and non standard retainers
 (3) Different shields and seals are available

⁽⁴⁾ Bearings also available with 1 or 2 shields/seals
 ⁽⁵⁾ Limiting speed also depends on seal, material and the respective ball complement

• Bearings without shields or retainers are also available with recesses.

 Almost all bearing types can also be enhanced with GRW XTRA. Detailed information you can find on page 79 and following. Please discuss your desired design in terms of flange, extended inner ring width, shield, lubrication, and material with our Technical Application Consultants to check availability.





GRW designation	[m]	nensions in nm] ich]	Bear Wldth without	ring without clos Width with extended	ure in [mm] [i Flange di without	mensions		aring with clos Width with extended	ure in [mm] [in Flange d with c	imensions	Chamfer in [mm] [inch]	to ANSI/AFE	limensions acc. BMA Std. 12.2 in [mm] i nch]		ngs acc. to) ⁽²⁾ (max)	Closure	options ⁽³⁾	Max. limiting sp	beed ⁽⁵⁾ [mm ⁻¹]
			closure	inner ring without closure	WINOU	ciosure	ciosure	inner ring with closure		losure		Shaft diameter	Housing diameter						
Basic symbol	d	D	В	B ₁	Flange diameter FD	Flange width FB	B ₂	B ₃	Flange diameter FD ₁	Flange width FB ₁	r _{s min} (1)	d _{a min}	D _{a max}	С [Ń]	C _{Or} [N]	Shield ⁽⁴⁾	Seal ⁽⁴⁾	without closure or with shield	with seal
9525	9.525	15.875	3.967	-	-	-	3.967	-	-	-	0.25	11.05	14.35	856	435	Х	-	35000	-
	.3750	.6250	.1562				.1562				.010	.435	.565						
3/8/002	9.525	22.225	-	-	-	-	5.558	-	-	-	0.41	11.45	20.30	2555	1129	Х	-	30000	-
	.3750	.8750					.2188				.016	.451	.799						
3/8	9.525	22.225	5.558	-	24.613	1.575	7.142	-	24.613	1.575	0.41	11.45	20.30	2555	1129	Х	Х	30000	24000
	.3750	.8750	.2188		.9690	.0620	.2812		.9690	.0620	.016	.451	.799						
12700A/002	12.700	19.050	-	-	-	-	3.967	-	-	-	0.25	14.20	17.55	918	542	Х	Х	28000	20000
	.5000	.7500					.1562				.010	.500	.691						
12700B	12.700	22.225	7.142	-	-	-	7.142	-	-	-	0.41	14.20	20.30	1972	1144	Х	-	28000	-
	.5000	.8750	.2812				.2812				.016	.500	.799						
1/2	12.700	28.575	6.350	-	31.115	1.575	7.938	-	31.115	1.575	0.41	15.90	26.05	5108	2413	Х	Х	32000	21000
	.5000	1.1250	.2500		1.2250	.0620	.3125		1.2250	.0620	.016	.626	1.026						
15875A	15.875	22.225	3.967	-	-	-	3.967	-	-	-	0.25	19.05	20.30	1133	801	Х	-	25000	_
	.6250	.8750	.1562				.1562				.010	.750	.799						
5/8	15.875	34.925	7.142	-	-	-	8.733	-	37.846	1.745	0.80	19.05	31.75	5999	3265	Х	-	25000	-
	.6250	1.3750	.2812				.3438		1.4900	.0687	.031	.750	1.250						

Note:

(1) f_{s min} = minimum single bearing chamfer or maximum permissible shaft or housing fillet radius
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 (3) Different shields and seals are available

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⁽⁵⁾ Limiting speed also depends on seal, material and the respective ball complement

• Bearings without shields or retainers are also available with recesses.

Please discuss your desired design in terms of flange, extended inner ring width, shield, lubrication, and material with our Technical Application Consultants to check availability.



• Subject to change.

Almost all bearing types can also be enhanced with GRW XTRA. Detailed information you can find on page 79 and following.



Spindle / angular contact bearings

Spindle bearings are single-row angular contact bearings with a nominal contact angle of 15° (C) or 25° (E). They can be subjected to both radial and (in one direction) axial loads. The direction of the axial load is shown by a "V" marking on the outer ring. GRW spindle ball bearings are suitable for applications requiring precision while carrying high load combined with high speed.

GRW spindle ball bearings are characterized by following properties:

- Manufactured quality of P4 (ABEC7) or better.
- Rings mostly made of corrosion-resistant SV 30 highgrade steel (other materials on request).
- Steel or ceramic balls.
- Solid retainer made from fiber-reinforced phenolic resin or special materials, for special applications, speed, etc...
- 15° (C) or 25° (E) contact angles as standard.
- Optionally, bearings can be paired with three pre-defined preload classes (L, M, S) or to a specific preload.
- Oil or grease lubrication.
- Open and shielded versions available.
- Cleanroom assembly, lubrication and packaging.



Open spindle ball bearings

- Standard configuration has large balls for optimum utilization of bearing geometries and a solid retainer for higher bearing capacities.
- The outer ring has only one partial shoulder remaining. This partial shoulder is necessary to prevent the bearing from separation.
- Solid outer ring guided retainer with a low profile crosssection is particularly well suited for oil injection lubrication or oil mist.

Shielded spindle bearings

- Non-contact shields do not cause any additional torque caused by the shields.
- Standard shields made of Viton (VZ) coupled with a stainless steel support shield offer excellent temperature and contamination resistance.
- A very small, closely toleranced sealing gap provides protection against dust particles.
- GRW recommends using a grease lubricant for longer life and reliability.
- Dimensionally identical to non-shielded spindle bearings but sometimes different inner geometry.
- This type of design often requires use of smaller balls that results in a lower load capacity but higher axial stiffness and speed limits (usually signified by A or B after the base type).
- Also available without shields for high-speed applications.

Handling

- GRW recommends leaving the bearing in its airtight packaging until you are ready for assembly.
- Extreme cleanliness during assembly is recommended.
- Avoid to drop or to subject the bearing to any kind of impact loading.
- Spindle bearings are designed to withstand axial loads in only one direction. This direction is identified by the "V" laser marking on the outer ring.
- Using the proper assembly tooling will prevent damage of the bearing.
- Duplex bearings labeled (DB), (DF), or (DT) are always packed in pairs and can only be used as pair in the specified configuration.
- Universally ground duplex bearings can be used in a combination of configurations, i.e. you can combine bearings from different packages or lots. These bearings may be assembled in any duplex arrangement.
- Prior to using these bearings in application GRW has found that a run in period at high speed helps to distribute the lubricant and is beneficial for the bearing.

Duplex bearings

Duplex bearings are two matched bearings that provide following performance benefits:

- Accurate bearing alignment in radial and axial directions including defined clearances and controlled stiffnesses.
- Increased system reliability.
- Higher load capacity.

Duplexing of these bearings is performed by loading each bearing with with a specified preload and accurately grinding the inner and/or outer rings until the bearing faces of both rings are flush.

Paired bearings processed this way are designed to be assembled in following configurations: backto-back (DB), face-to-face (DF) or tandem (DT) and axially loaded to the specified or required force. Duplexed bearings are designed to provide the specified preload when the ground surfaces are accurately pressed together.

The ball bearings must be mounted according to the designation on the packaging labels or "V" markings on the outer rings.





Deep groove radial bearings:

For deep groove duplex bearings, the radial play is larger than normal to facilitate the desired contact angle, rigidity, and axial load capacity.

Unless otherwise specified, GRW duplex grinds deep groove radial bearings to a preload of 5 N and a nominal contact angle of 15°. If necessary, preload and contact angles can be adjusted to a customer's unique operating requirements.

Spindle bearings:

Preload and contact angle are generally standardized for spindle bearings. GRW's standard contact anales are 15° (C) or 25° (E), preload is specified as light (L), medium (M) or heavy (S). If necessary, preload and contact angles can be customized to each customer's individual operating requirements.

	By default, GRW uses for:	
	Deep groove radial bearings	Spindle bearings
Contact angle α	15° (C)	15° (C) or 25° (E)
Preload FV	5 N	L, M, S

However, the preload should not be specified higher than necessary as this would result in an increase of start up and running torque, which in turn would directly affect the expected life of the bearing.

To achieve, an identical fit for both bearings, Duplex bearings are sorted into two groups. The bore and outer diameters are packaged in pairs with bearings from the same group. To take full advantage of these duplexed pairs, they should also be mounted with calibrated shafts and housings (see chapter "Calibration of bore and outside diameters")

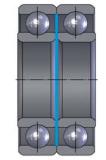
Bearing fits should be carefully selected because an interference fit on the inner or outer ring will change the preload.



Installation and configuration of duplex bearings

O (<>) arrangement: Back to back (designation -1 and DB for spindle bearings)

With this bearing configuration, the inner rings are designed to be clamped together. The contact angle load path between the outer ring raceway, the ball and the inner ring raceway diverge, which results in maximum stability and stiffness against any moment loading. Radial and axial loads can be taken in both directions.



X (><) arrangement: Face to face (designation -2 and DF for spindle bearings)

With this bearing configuration, the outer rings are designed to be clamped together. The load path converges resulting in less stability and a lower stiffness against moment loading. This design more easily compensates for any misalignment of the assembly. Radial and axial loads can likewise be taken in both directions.

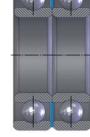
Tandem (>>) or (<<) arrangement (designation -3 and DT for spindle bearings)

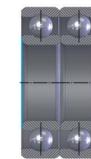
The tandem-mounted bearing design is capable of taking a significantly higher axial load, but only in one direction. With this type of bearing, preloading and control of axial play can only be achieved by preloading against another bearing pair.

General: Bearings with these pairing configurations are packed in pairs or sets and must not be mixed.

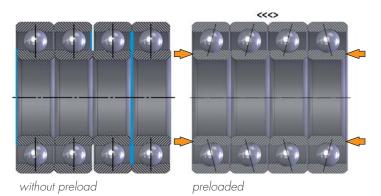
Universal (designation -4 and U for spindle bearings)

Universally matched bearing pairs have a significant advantage compared to the duplexed designs described above. They are individually ground in such a way that they can be assembled in various pairing configurations, e.g. X, O, or tandem configuration without any loss in performance. With the same preload, these single bearings can be interchanged without any problems.





without preload



Bearing sets

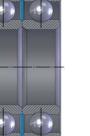
When a higher stiffness is specified, multiple duplexed bearing configurations may be used together to achieve the desired results. Depending on the application, these bearing sets can be made of universally

	Usual designation	Mark/ arrangement	Permissible load direction	Stiffness
(4) (4) (4) (4) (4) (4)	O arrangement -1 or DB	<>	axial radial	axial radial rigidity against moving torques
	X arrangement −2 or DF	><	axial radial	axial radial
(4) (4) (4) (4) (4) (4)	Tandem arrangement −3 or DT	<< or >>	radial and one direction axially	unilaterally axial radial
	Universal −4 or U	<<>< Examples: >< or <> or >> or	axial radial	depending on the configuration
	Set of bearings assem- bled from universally matched bearings	><< Examples: <>>		depending on the configuration

Superduplex bearings

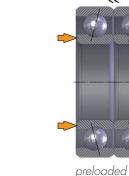
For Superduplex bearings, the following configurations apply: Superduplex bearings are double-row deep groove radial bearings or angular contact bearings where either Designation –5 the inner or outer rings are integral and the remaining rings are separate to allow for assembly and proper • Designation -6 pre-loading. (See also chapter "Special bearings" \rightarrow Superduplex bearings or Extraduplex bearings).

without preload



without preload





preloaded

preloaded



paired bearings in X, O, or tandem configurations. The table below shows some examples of potential, configurations in more detail.

- O(<>) configuration (corresponds to designation -1)
- X (><) configuration (corresponds to designation -2)
- Designation –7 Tandem (corresponds to designation -3)



Designation system for spindle ball bearings

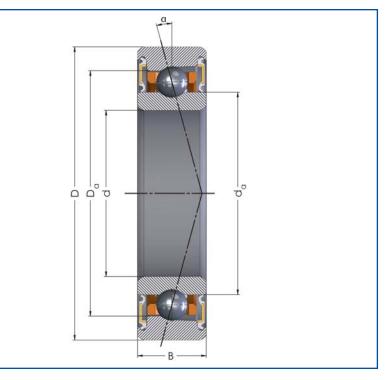


	Ball material		Ring material		Basic mark		Closure		Contact angle		Quality class
	-		-		705		-		С		P4
	HY		SS		7000		-Z		E		P4S
	ZO		SV		795		-2Z		D = °		
					7900		-VZ				
					705 B		-2VZ				
-	steel balls	-	100Cr6	70	Series 10	-	open ball bearing	с	15°	P4	acc. to DIN 620-2
нү	ceramic	SS	X65Cr13	79	Series 19	-Z	one metal shield	E	25°	P4S	dimension accuracy P4, running accuracy P2,
	balls made of Si ₃ N ₄	sv	X30CrMoN 15-1 Standard	705 b	Modified internal design	-2Z	two metal shields		er contact gles available		acc. to DIN 620-2
	01 0131 44		Sidildala		memar design	-VZ	one Viton shield	on	request, . D = 20°		
ZO	ceramic balls made of ZrO ₂					-2VZ	two Viton shields	e.y	. D = 20		
						All Va closur	riants are non-contact es				



	Retainer design	D	iameter grading		Duplex type		Preload value	Lu	bricant quantity	L	ubricants
	TA		-				-				-
	TB		Х		U		L		%		L
	AC2TA		ХВ		DB		Μ				G
	L2TA		XD		DF		S				L299
			X4		DT		/X				
			X4B								
			X4D								
TA	solid retainer made of fiber-reinforced phenolic resin guided	-	without diameter grading	-	single bearing not duplexed	-	without preload	-	Standard grease quantitiy 20 % of free bearing	-	open bearings are preserved with oil LOO1,
	by outer ring	x	bore and outside diameter graded in	U	universally duplexed	L	light		volume with closed spindle		closed bearings are
TB	same as TA, with quide at inner ring		2 classes			Μ	medium		bearing		greased with 20% grease
-		XB	bore graded in	Bea	ring pair:	S	heavy	%	adjusted lubricant		0.510
TXA	other retainer materials available		2 classes	DB	2 bearings in	/x	preload		quantity in [%] of free bearing		G510 as a standard
	on request	XD	outside diameter		O arrangement	/^	value in [N]		volume		sianaara
			graded in 2 classes		0		if other than			L	Oil
-TA	angular contact			DF	2 bearings in		L, M, S.				
-TB	shoulder on outer ring (standard)	X4	bore and outside diameter graded		X arrangement					G	Grease
			in 4 classes	DT	2 bearings in						
AC2	angular contact shoulder on inner ring	X4B	bore graded in 4 classes		Tandem arrangement					L299	dry bearing
l2ta	inner ring can be dismounted, solid retainer keeps the balls from falling out	X4D	outside diameter graded in 4 classes			bear (= ur	nple: Spindle ball ing U/10 iiversally paired 10 N preload)				







Spindle bearings

GRW designation	M	ain dimensior [mm]	is in		ratings DIN ISO		Ball set	Limiting s	peeds*		Preload	
Basic symbols	d	[inch] D	В	C _{or} [N]	C _r [N]	Z	Dw [mm] [inch]	Oil [min ⁻¹]	Grease [min ⁻¹]	(L) light [N]	(M) medium [N]	(S) heavy [N]
C bearings, open, m	etric											
SV723 C TA	3.00 .1181	10.00 .3937	4.00 .1575	170	506	8	1.588 .0625	254000	209000	5	8]
HYSV723 C TA	3.00 .1181	10.00 .3937	4.00 .1575	119	506	8	1.588 .0625	373000	269000	5	8	1
SV774 C TA	4.00 .1575	7.00 .2756	2.00 .0787	77	223	10	1.000 .0394	309000	255000	5	7	1
HYSV774 C TA	4.00 .1575	7.00 .2756	2.00 .0787	54	223	10	1.000 .0394	455000	327000	5	7]
SV724 C TA	4.00 .1575	13.00 .5118	5.00 .1969	364	1037	8	2.381 .0937	195000	161000	5	16	3
HYSV724 C TA	4.00 .1575	13.00 .5118	5.00 .1969	255	1037	8	2.381 .0937	287000	206000	5	16	3
SV734 C TA	4.00 .1575	16.00 .6299	5.00 .1969	721	1594	9	2.500 .0984	1 <i>57</i> 000	130000	8	24	4
HYSV734 C TA	4.00 .1575	16.00 .6299	5.00 .1969	504	1594	9	2.500 .0984	231000	167000	8	24	4
SV725 C TA	5.00 .1969	16.00 .6299	5.00 .1969	721	1594	9	2.500 .0984	1 <i>57</i> 000	130000	8	24	4
HYSV725 C TA	5.00 .1969	16,00 .6299	5.00 .1969	504	1594	9	2.500 .0984	231000	167000	8	24	2
SV735 C TA	5.00 .1969	19.00 .7480	6.00 .2362	1277	2612	10	3.175 .1250	127000	105000	13	40	8
HYSV735 C TA	5.00 .1969	19.00 .7480	6.00 .2362	894	2612	10	3.175 .1250	187000	135000	13	40	8
SV786 C TA	6,00 .2362	13.00 .5118	3.50 .1378	354	895	10	1.984 .0781	175000	144000	5	14	2
HYSV786 C TA	6.00 .2362	13 .5118	3.50 .1378	247	895	10	1.984 .0781	258000	186000	5	14	4
SV786 E TA	6.00 .2362	13.00 .5118	3.50 .1378	332	856	10	1.984 .0781	149000	123000	5	14	4
HYSV786 E TA	6.00 .2362	13.00 .5118	3.50 .1378	232	856	10	1.984 .0781	219000	158000	5	14	2
SV786/001 C TA	6.00 .2362	13.00 .5118	5.00 .1969	354	895		1.984 .0781	175000	144000	5	14	2
HYSV786/001 C TA	6.00 .2362	13.00 .5118	5.00 .1969	247	895	10	1.984 .0781	258000	186000	5		4
SV726 C TA	6.00 .2362	19.00 .7480	6.00 .2362	1277	2612	10	3.175 .1250	127000	105000	13	40	8
HYSV726 C TA	6.00 .2362	19.00 .7480	6.00 .2362	894	2612	10	3.175 .1250	187000	135000	13		8
SV707 C TA HYSV707 C TA	7.00 .2756	19.00 .7480	6.00 .2362	1277 894	2612 2612	10 10	3.175 .1250	127000	105000	13	40	8
SV727 C TA	7.00 .2756 7.00	19.00 .7480 22.00	6.00 .2362 7.00	1693	3511	9	3.175 .1250 3.969	187000	95000	13	40 54	10
	.2756	.8661	.2756				.1563					
HYSV727 C TA	7.00 .2756	22.00 .8661	7.00 .2756	1185	3511	9	3.969 .1563	170000	122000	18	54	10
SV788 C TA	8.00 .3150	16.00 .6299	4.00 .1575	569	1377	10	2.500 .0984	142000	117000	7	21	4

RVV esignation	Main dimensions in [mm] [inch]			Load ratings Ball set acc. to DIN ISO				Limiting s	Preload			
asic symbols	d	D	В	C _{or} [N]	C, [N]	Z	Dw [mm] [inch]	Oil [min ⁻¹]	Grease [min ⁻¹]	(L) light [N]	(M) medium [N]	(S) heavy [N]
bearings, open, m	netric											
HYSV788 C TA	8.00	16.00	4.00	398	1377	10	2.500	208000	150000	7	21	4
	.3150	.6299	.1575				.0984					
SV788 E TA	8.00	16.00	4.00	534	1317	10	2.500	120000	99000	7	21	2
	.3150	.6299	.1575				.0984					
HYSV788 E TA	8.00	16.00	4.00	374	1317	10	2.500	177000	128000	7	21	4
	.3150	.6299	.1575				.0984					
SV708 C TA	8.00	22.00	7.00	1693	3511	9	3.969	116000	95000	18	54	10
	.3150	.8661	.2756				.1563					
HYSV708 C TA	8.00	22.00	7.00	1185	3511	9	3.969	170000	122000	18	54	10
	.3150	.8661	.2756				.1563					
SV708 E TA	8.00	22.00	7.00	1589	3358	9	3.969	98000	81000	18	54	1(
	.3150	.8661	.2756		0.0.5.0	0	.1563	1.450.00	10.4000	1.0	5.4	
HYSV708 E TA	8.00	22.00	7.00	1112	3358	9	3.969	145000	104000	18	54	1(
0./700.0.74	.3150	.8661	.2756	(10	1 (7)	1.1	.1563	101000	100000	0		-
SV789 C TA	9.00	17.00	4.00	642	1471	11	2.500	131000	108000	8	23	4
	.3543	.6693	.1575	4.5.0	1 4 7 1	1.1	.0984	100000	100000	0		
HYSV789 C TA	9.00	17.00	4.00	450	1471	11	2.500	192000	138000	8	23	2
	.3543	.6693	.1575	1074	0044	10	.0984	105000			50	
SV709 C TA	9.00	24.00	7.00	1974	3844	10	3.969	105000	86000	20	59	1
	.3543	.9449	.2756	1000	0044	10	.1563	154000	111000	00	20 59 20 59 20 79	1
HYSV709 C TA	9.00	24.00	7.00	1382	3844	10	3.969	154000	111000	20	20 59	1
SV729 C TA	.3543 9.00	.9449 26.00	.2756 8.00	2737	5137	10	.1563 4.763	94000	78000	26	7 21 7 21 3 54 3 54 3 54 3 54 3 54 3 54 3 54 3 54 3 23 3 23 0 59 5 79 5 79 5 79 3 24 3 24 3 24 5 44 5 44	1.
SVZAC IA	.3543	1.0236	.3150	2/3/	5157	10	4.703 .1875	94000	78000	20	14	
HYSV729 C TA	9.00	26.00	8.00	1916	5137	10	4.763	139000	100000	26	70	1.
HISV/ZYC IA	.3543	1.0236	.3150	1410	3137	10	4.703 .1875	139000	100000	20	/ 4	1.
SV7800 C TA	10.00	19.00	5.00	724	1556	12	2.500	117000	97000	8	24	
377000 C 1A	.3937	.7480	.1969	/ 24	1550	ΙZ	.0984	117000	97000	0	24	1
HYSV7800 C TA	10.00	19.00	5.00	507	1556	12	2.500	172000	124000	8	24	
111377000 C 1A	.3937	.7480	.1969	507	1550	ΙZ	.0984	17 2000	124000	0	24	
SV7800 E TA	10.00	19.00	5.00	680	1488	/12	2.500	100000	82000	8	24	
017 000 L 171	.3937	.7480	.1969	000	1400	12	.0984	100000	02000	U	27	
HYSV7800 E TA	10.00	19.00	5.00	476	1488	12	2.500	147000	106000	8	24	
11100/0000 2 1/1	.3937	.7480	.1969	17 0	1 100	12	.0984	1 17 0000	100000	Ŭ	21	
SV7900 C TA	10.00	22.00	6.00	1500	2824	11	3.175	107000	88000	15	44	
0,,,,00,0,,,,	.3937	.8661	.2362		2021		.1250	10,000	Base		NAD	XX
HYSV7900 C TA	10.00	22.00	6.00	1050	2824	11	3.175	157000	113000	15	medium 7 21 7 21 7 21 3 54 3 54 3 54 3 54 3 54 3 54 3 54 3 54 3 54 3 54 3 54 3 23 5 79 5 79 5 79 6 79 7 24 3 24 3 24 3 24 5 44 5 44	NY 73
	.3937	.8661	.2362				.1250					
SV7900A E TA	10.00	22.00	6.00	1407	2700	11	3.175	90000	74000	15	44	
	.3937	.8661	.2362		1-		.1250	10 A	THE			
HYSV7900A E TA	10.00	22.00	6.00	985	2700	11	3.175	133000	96000	15	3 54 3 54 3 54 3 54 3 54 3 54 3 23 3 23 3 23 5 79 5 79 6 79 6 79 7 24 3 24 3 24 3 24 5 44 5 44	
	.3937	.8661	.2362				.1250					
SV7000 C TA	10.00	26.00	8.00	2737	5137	10	4.763	94000	78000	26	 21 54 54 54 54 54 23 23 23 29 59 59 79 24 44 44 44 79 	1.
	.3937	1.0236	.3150		7		.1875	HIN				
HYSV7000 C TA	10.00	26.00	8.00	1916	5137	10	4.763	139000	100000	26	79	1.
	.3937	1.0236	.3150				.1875					

* The indicated speed limits are guidelines for spring-loaded single bearings with low loads; depending on the respective application, higher or lower speed limits may apply in application.

• Subject to change. Additional types on request!



** For use with oil lubrication, these bearings are also available without shields.
Almost all bearing types can also be enhanced with GRVV XTRA. Detailed information you can find on page 79 and following.



Spindle bearings

GRW designation	Mo	ain dimension [mm] [inch]	is in	Load r acc. to [atings DIN ISO		Ball set	Limiting s	peeds*		Preload	
Basic symbols	d	[inch] D	В	C _{or} [N]	C _r [N]	Z	Dw [mm] [inch]	Oil [min ⁻¹]	Grease [min ⁻¹]	(L) light [N]	(M) medium [N]	(S) heavy [N]
C bearings, open, m	etric											
SV7000 E TA	10.00 .3937	26.00 1.0236	8.00 .3150	2568	4913	10	4.763 .1875	80000	66000	26	79	15
HYSV7000 E TA	10.00	26.00	8.00	1798	4913	10	4.763	118000	85000	26	79	15
SV7200 C TA	.3937 10.00	1.0236 30.00	.3150 9.00	3192	5597	11	.1875 4.763	83000	68000	29	86	17
HYSV7200 C TA	.3937 10.00	1.1811 30.00	.3543 9.00	2235	5597	11	.1875 4.763	122000	88000	29	86	17
1113W 200 C 1A	.3937	1.1811	.3543	2233	5547	11	.1875	122000	00000		00	
SV7200 E TA	10.00 .3937	30.00 1.1811	9.00 .3543	2995	5353	11	4.763 .1875	71000	58000	29	86	17
HYSV7200 E TA	10.00 .3937	30.00 1.1811	9.00 .3543	2097	5353	11	4.763 .1875	104000	75000	29	86	17
SV7801 C TA	12.00 .4724	21.00 .8268	5.00 .1969	794	1543	14	2.381 .0937	103000	84000	8	24	4
HYSV7801 C TA	12.00	21.00	5.00	556	1543	14	2.381	151000	109000	8	24	2
SV7801 E TA	.4724 12.00	.8268 21.00	.1969 5.00	745	1476	14	.0937 2.381	87000	72000	8	24	1
HYSV7801 E TA	.4724 12.00	.8268 21.00	.1969 5.00	521	1476	14	.0937 2.381	128000	92000	8	24	4
SV7901 C TA	.4724 12.00	.8268 24.00	.1969 6.00	1700	2992	12	.0937 3.175	94000	78000	15	46	(
HYSV7901 C TA	.4724 12.00	.9449 24.00	.2362 6.00	1190	2992	12	.1250 3.175	139000	100000	15	46	(
SV7901 E TA	.4724 12.00	.9449 24.00	.2362 6.00	1595	2861	12	.1250 3.175	80000	66000	15	46	
HYSV7901 E TA	.4724 12.00	.9449 24.00	.2362 6.00	1117	2861	12	.1250 3.175	118000	85000	15	46	
SV7001 C TA	.4724 12.00	.9449 28.00	.2362 8.00	2590	4423	12	.1250 3.969	82000	68000	23	68	1
	.4724	1.1024	.3150				.1563					
hysv7001 c ta	12.00 .4724	28.00 1.1024	8.00 .3150	1813	4423	12	3.969 .1563	121000	87000	23	68	1
SV7001 E TA	12.00 .4724	28.00 1.1024	8.00 .3150	2430	4230	12	3.969 .1563	70000	58000	23	68	1:
HYSV7001 E TA	12.00	28.00	8.00	1701	4230	12	3.969	103000	74000	23	68	1;
SV7201C C TA	.4724 12.00	1.1024 32.00	.3150 10.00	3806	7652	9	.1563 5.953	77000	64000	39	118	2
HYSV7201C C TA	.4724 12.00	1.2598 32.00	.3937 10.00	2664	7652	9	.2344 5.953	114000	82000	39	118	23
SV7201C E TA	.4724 12.00	1.2598 32.00	.3937 10.00	3571	7318	9	.2344 5.953	66000	54000	39	118	2
HYSV7201C E TA	.4724	1.2598	.3937	2500			.2344		70000	39	118	2
	12.00 .4724	32.00 1.2598	10.00 .3937	2500	7318		5.953 .2344	97000	70000			
SV7802 C TA	15.00 .5906	24.00 .9449	5.00 .1969	1054	1784	18	2.381 .0937	87000	72000	9	27	
HYSV7802 C TA	15.00 .5906	24.00 .9449	5.00 .1969	738	1784	18	2.381 .0937	128000	92000	9	27	
SV7802 E TA	15.00 .5906	24.00 .9449	5.00 .1969	989	1706	18	2.381 .0937	74000	61000	9	27	

GRVV lesignation	Ma	ain dimension [mm] [inch]	s in	Load I acc. to I	ratings DIN ISO		Ball set	Limiting s	peeds*	Preload		
asic symbols	d	D	В	C _{or} [N]	C _r [N]	Z	Dw [mm] [inch]	Oil [min ⁻¹]	Grease [min ⁻¹]	(L) light [N]	(M) medium [N]	(S) heavy [N]
C bearings, open, m	etric											
HYSV7802 E TA	15.00	24.00	5.00	692	1706	18	2.381	109000	78000	9	27	5.
	.5906	.9449	.1969				.0937					
SV7902 C TA	15.00	28.00	7.00	2841	4666	13	3.969	79000	65000	24	72	14
	.5906	1.1024	.2756	1000	A I I I	1.0	.1563	11/000	0.4000	0.4	70	1.4
HYSV7902 C TA	15.00	28.00	7.00	1989	4666	13	3.969	116000	84000	24	72	12
SV7902 E TA	.5906 15.00	1.1024 28.00	.2756 7.00	2665	4463	13	.1563 3.969	67000	55000	24	70	14
307902 E IA	.5906	1.1024	.2756	2665	4403	13	.1563	07000	33000	24	12	14
HYSV7902 E TA	15.00	28.00	7.00	1866	4463	13	3.969	99000	71000	24	72]2
THOW FOZE IA	.5906	1.1024	.2756	1000	4405	15	.1563	77000	71000	24	12	14
SV7002 C TA	15.00	32.00	9.00	3970	6327	13	4.763	72000	60000	32	97	19
017 002 0 17	.5906	1.2598	.3543	0 // 0	002/	10	.1875	, 2000	00000	02		
HYSV7002 C TA	15.00	32.00	9.00	2779	6327	13	4.763	106000	77000	32	97	19
	.5906	1.2598	.3543				.1875					
SV7002 E TA	15.00	32.00	9.00	3725	6051	13	4.763	62000	51000	32	97	19
	.5906	1.2598	.3543				.1875					
HYSV7002 E TA	15.00	32.00	9.00	2607	6051	13	4.763	90000	65000	32	97	19
	.5906	1.2598	.3543				.1875					
SV7202 C TA	15.00	35.00	11.00	4090	6970	13	4.763	97000	63000	30	60	12
	.5906	1.3780	.4331				.1875				15 90	
SV7202 E TA	15.00	35.00	11.00	3930	6650	13	4.763	85000	55000	45	45 90	18
01/7000 0 71	.5906	1.3780	.4331	1071	1754	1.0	.1875	70000	1.5000		4 72 4 72 4 72 4 72 4 72 4 72 4 72 4 72 2 97 2 97 2 97 2 97 2 97 2 97 2 97 2 97 2 97 2 97 2 97 2 97 2 97 2 97 2 97 2 97 2 97 2 27 2 27 2 27 2 27 2 27 2 27 2 75 5 75 5 75 5 75 5 75 5 75 5	
SV7803 C TA	17.00	26.00	5.00	1071	1754	18	2.381	79000	65000	9	27	
HYSV7803 C TA	.6693 17.00	1.0236 26.00	.1969 5.00	750	1754	10	.0937 2.381	114000	0.4000	0	07	1
HISV/803 C IA	.6693	1.0236	5.00 .1969	750	1734	18	2.38 .0937	116000	84000	9	27	
SV7803 E TA	.0093 17.00	26.00	5.00	1005	1677	18	2.381	67000	55000	9	27	
377003 L IA	.6693	1.0236	.1969	1005	10/7	10	.0937	0/000	55000	4	21	
HYSV7803 E TA	17.00	26.00	5.00	704	1677	18	2.381	99000	71000	9	27	1
	.6693	1.0236	.1969	, 0 1	10/ /	10	.0937	,,,,,,,,	, 1000		2/	
SV7903 C TA	17.00	30.00	7.00	3137	4888	14	3.969	72000	60000	25	75	15
	.6693	1.1811	.2756		14		.1563			Sector 1		
HYSV7903 C TA	17.00	30.00	7.00	2196	4888	14	3.969	106000	77000	25	75	15
	.6693	1.1811	.2756				.1563					
SV7903 E TA	17.00	30.00	7.00	2944	4675	14	3.969	61000	51000	25	75	J.
	.6693	1.1811	.2756	1 PE		A	.1563		POX	J.		MA.
HYSV7903 E TA	17.00	30.00	7.00	2061	4675	14	3.969	90000	65000	25	75	15
	.6693	1.1811	.2756				.1563					
SV7003 C TA	17.00	35.00	10.00	4571	6817	14	4.763	65000	54000	34	102	20
	.6693	1.3780	.3937	0000	(0)7	1.4	.1875	0/000		0.4	100	
HYSV7003 C TA	17.00	35.00	10.00	3200	6817	14	4.763	96000	69000	34	102	20
	.6693	1.3780	.3937	1571	6017	1.4	.1875	54000	14000	0.4	100	00
SV7003 E TA	17.00 .6693	35.00 1.3780	10.00 .3937	4571	6817	14	4.763 .1875	56000	46000	34	102	20
HYSV7003 E TA	.0093 17.00	35.00	10.00	3200	6817	14	4.763	82000	59000	34	102	20
1113V/003 E 1A	.6693	35.00 1.3780	.3937	5200	0017	14	4.703 .1875	62000	39000	34	102	20

* The indicated speed limits are guidelines for spring-loaded single bearings with low loads; depending on the respective application, higher or lower speed limits may apply in application.

• Subject to change. Additional types on request!



** For use with oil lubrication, these bearings are also available without shields.
Almost all bearing types can also be enhanced with GRVV XTRA. Detailed information you can find on page 79 and following.



Spindle bearings

GRW designation	Mc	ain dimension [mm] [inch]	s in		ratings DIN ISO		Ball set	Limiting s	peeds*	Preload		
Basic symbols	d	D	В	C _{or} [N]	C _r [N]	Ζ	Dw [mm] [inch]	Oil [min ⁻¹]	Grease [min ⁻¹]	(L) light [N]	(M) medium [N]	(S) heavy [N]
C bearings, open, m	etric											
SV7203 C TA	17.00	40.00	12.00	5090	8730	12	5.556	85000	55000	35	70	14
	.6693	1.5748	.4724				.2187					
SV7203 E TA	17.00	40.00	12.00	4860	8340	12	5.556	75000	49000	60	120	24
	.6693	1.5748	.4724				.2187					
SV7804 C TA	20.00	32.00	7.00	2772	3772	18	3.175	65000	54000	19	58	11
	.7874	1.2598	.2756	1041	3772	1.0	.1250	04000	40000	19	58	11
HYSV7804 C TA	20.00 .7874	32.00 1.2598	7.00 .2756	1941	3//2	18	3.175 .1250	96000	69000	19	30	11
SV7804 E TA	20.00	32.00	7.00	2870	3865	18	3.175	56000	46000	19	58	11
377004 L 1A	.7874	1.2598	.2756	2070	3000	10	.1250	50000	40000	17	50	11
HYSV7804 E TA	20.00	32.00	7.00	2009	3772	18	3.175	82000	59000	19	58	11
11100/004 2 1/(.7874	1.2598	.2756	2007	0772	10	.1250	02000	07000	17	00	
SV7904 C TA	20.00	37.00	9.00	4854	7543	15	4.763	60000	49000	39	116	23
	.7874	1.4567	.3543				.1875					
HYSV7904 C TA	20.00	37.00	9.00	3398	7543	15	4.763	88000	63000	39	116	23
	.7874	1.4567	.3543				.1875					
SV7904 E TA	20.00	37.00	9.00	4554	7214	15	4.763	51000	42000	39	116	23
	.7874	1.4567	.3543				.1875					
HYSV7904 E TA	20.00	37.00	9.00	3188	7214	15	4.763	75000	54000	39	116	23
	.7874	1.4567	.3543				.1875					
SV7004 C TA	20.00	42.00	12.00	6090	9660	14	5.556	75000	49000	35	70	14
	.7874	1.6535	.4724				.2187					
SV7004 E TA	20.00	42.00	12.00	5810	9210	14	5.556	66000	43000	55	110	22
sv7204 c ta	.7874	1.6535 47.00	.4724	7200	11700	13	.2187	72000	47000	45	90	18
5V7 204 C TA	20.00 .7874	47.00 1.8504	14.00 .5512	7320	11700	13	6.350 .2500	/2000	47000	43	90	18
SV7204 E TA	20.00	47.00	14.00	7010	11100	13	6.350	63000	41000	70	140	28
317 204 L IA	.7874	1.8504	.5512	7010	11100	10	.2500	03000	41000	/0	140	20
SV7805 C TA	25.00	37.00	7.00	2335	3397	19	3.175	55000	45000	17	52	10
017 000 0 171	.9843	1.4567	.2756	2000	00//	. /	.1250	00000	10000	17	02	10
HYSV7805 C TA	25.00	37.00	7.00	1634	3397	19	3.175	81000	58000	17	52	10
	.9843	1.4567	.2756				.1250					
SV7005 C TA	25.00	47.00	12.00	6918	11769	12	6.747	47000	39000	59	177	35
	.9843	1.8504	.4724				.2656					
HYSV7005 C TA	25.00	47.00	12.00	4843	11769	12	6.747	69000	50000	59	177	35
	.9843	1.8504	.4724				.2656					
SV7005 E TA	25.00	47.00	12.00	6890	9920	16	5.556	57000	37000	55	110	22
	.9843	1.8504	.4724				.2187					
(SV)7205 C TA	25.00	52.00	15.00	8710	12800	15	6.350	63000	41000	50	100	20
	.9843	2.0472	.5906	0.000	10100	1 -	.2500	E 5000	0/000	000	1/0	0.0
(SV)7205 E TA	25.00	52.00	15.00	8330	12100	15	6.350	55000	36000	80	160	32
	.9843	2.0472	.5906	0010	12100	17	.2500	55000	26000	10	00	14
(SV)7006 C TA	30.00 1.1811	55.00 2.1654	13.00 .5118	9010	12100	17	5.953 .2344	55000	36000	40	80	16
(SV)7006 E TA	30.00	55.00	13.00	8560	11500	17	.2344 5.953	48000	31000	65	130	26
(317 000 L 1A	1.1811	2 .1654	.5118	0500	11300	17	3.933 .2344	40000	51000	05	130	20

GRW designation	Mc	ain dimension: [mm] [inch]	s in	Load r acc. to [atings DIN ISO		Ball set	Limiting s	peeds*		Preload	
Basic symbols	d	D	В	C _{or} [N]	C _r [N]	Z	Dw [mm] [inch]	Oil [min ⁻¹]	Grease [min ⁻¹]	(L) light [N]	(M) medium [N]	(S) heavy [N]
AC bearings, open, in	ch											
SV3/16C TA	4.763 .1875	12.700 .5000	3.967 .1562	312	913	8	2.381 .0937	195000	161000	5	14	28
HYSV3/16C TA	4.763 .1875	12.700 .5000	3.967 .1562	218	913	8	2.381 .0937	287000	206000	5	14	28
SV3/16 D TA	4.764 .1876	12.800 .5039	3.967 .1562	293	873	8	2.381 .0937	166000	136000	5	14	28
HYSV3/16 D TA	4.765 .1876	12.900 .5079	3.967 .1562	205	873	8	2.381 .0937	244000	175000	5	14	28
SV1/4AC TA	6.350 .2500	15.875 .6250	4.978 .1960	421	1114	9	2.500 .0984	153000	126000	6	17	34
HYSV1/4A C TA	6.350 .2500	15.875 .6250	4.978 .1960	295	1114	9	2.500 .0984	225000	162000	6	17	34
SV1/2/001 C TA	12.700 .5000	28.575 1.1250	7.938 .3125	2063	4066	12	3.969 .1563	82000	68000	20	61	121
HYSV1/2/001 C TA	12.700 .5000	28.575 1.1250	7.938 .3125	1444	4066	12	3.969 .1563	121000	87000	20	61	121

GRW designation	Mc	ain dimension: [mm] [inch]	s in	Load r acc. to [atings DIN ISO		Ball set	Limiting s	peeds*		Preload	
Basic symbols	d	D	В	C _{or} [N]	C, [N]	Z	Dw [mm] [inch]	Oil [min ⁻¹]	Grease [min ⁻¹]	(L) light [N]	(M) medium [N]	(S) heavy [N]
AC bearings, open, in	ch											
SV3/16C TA	4.763 .1875	12.700 .5000	3.967 .1562	312	913	8	2.381 .0937	195000	161000	5	14	28
HYSV3/16C TA	4.763 .1875	12.700 .5000	3.967 .1562	218	913	8	2.381 .0937	287000	206000	5	14	28
SV3/16 D TA	4.764 .1876	12.800 .5039	3.967 .1562	293	873	8	2.381 .0937	166000	136000	5	14	28
hysv3/16 d ta	4.765 .1876	12.900 .5079	3.967 .1562	205	873	8	2.381 .0937	244000	175000	5	14	28
SV1/4AC TA	6.350 .2500	15.875 .6250	4.978 .1960	421	1114	9	2.500 .0984	153000	126000	6	17	34
HYSV1/4A C TA	6.350 .2500	15.875 .6250	4.978 .1960	295	1114	9	2.500 .0984	225000	162000	6	17	34
SV1/2/001 C TA	12.700 .5000	28.575 1.1250	7.938 .3125	2063	4066	12	3.969 .1563	82000	68000	20	61	121
HYSV1/2/001 C TA	12.700 .5000	28.575 1.1250	7.938 .3125	1444	4066	12	3.969 .1563	121000	87000	20	61	121

AC bearings, dismountable, metric and inch

SV784 D L2T	4.00	9.00	2.50	132	457	7	1.588	242000	199000	5	8	15
	.1575	.3543	.0984				.0625					
HYSV784 D L2T	4.00	9.00	2.50	94	457	7	1.588	355000	256000	5	8	15
	.1575	.3543	.0984				.0625					
SV725 C L2T	5.00	16.00	5.00	737	1626	9	2.500	1 <i>5</i> 7000	130000	8	24	49
	.1969	.6299	.1969				.0984					l Ma
HYSV725 C L2T	5.00	16.00	5.00	515	1626	9	2.500	231000	167000	8	24	49
	.1969	.6299	.1969				.0984					
SV725 D L2T	5.00	16.00	5.00	737	1626	9	2.500	134000	110000	8	24	49
	.1969	.6299	.1969				.0984					
HYSV725 D L2T	5.00	16.00	5.00	515	1626	9	2.500	197000	142000	8	24	49
	.1969	.6299	.1969				.0984					
SV707 C L2T	7.00	19.00	6.00	1183	2617	10	3.175	127000	105000	13	40	80
	.2756	.7480	.2362		12		.1250					
HYSV707 C L2T	7.00	19.00	6.00	828	2617	10	3.175	187000	135000	13	40	80
	.2756	.7480	.2362				.1250					
SV7000 C L2T	10.00	26.00	8.00	2550	4906	10	4.763	94000	78000	28	85	170
	.3937	1.0236	.3150	M		A	.1875		AAX	JA	YW	VA/
HYSV7000 C L2T	10.00	26.00	8.00	1785	4906	10	4.763	139000	100000	28	85	170
	.3937	1.0236	.3150				.1875					
SV1/8A D20 L2T	3.175	7.938	2.779	207	609	7	1.588	266000	219000	5	8	16
	.1250	.3125	.1094		H		.0625		NAM			
HYSV1/8A D20 L2T	3.175	7.938	2.779	144	609	7	1.588	392000	282000	5	8	16
	.1250	.3125	.1094				.0625					
SV1/8B D20 L2T	3.175	9.525	3.967	134	461	8	1.588	228000	188000	5	10	20
	.1250	.3750	.1562	1	1		.0625	H12				
HYSV1/8B D20 L2T	3.175	9.525	3.967	95	461	8	1.588	336000	242000	5	10	20
	.1250	.3750	.1562				.0625					

* The indicated speed limits are guidelines for spring-loaded single bearings with low loads; depending on the respective application, higher or lower speed limits may apply in application.

• Subject to change. Additional types on request!



** For use with oil lubrication, these bearings are also available without shields.
Almost all bearing types can also be enhanced with GRW XTRA. Detailed information you can find on page 79 and following.



Spindle bearings

GRW designation	Ma	ain dimension [mm]	s in	Load r acc. to [Ball set	Limiting s	speeds*		Preload	
Basic symbols	d	[inch] D	В	C _{or} [N]	C _r [N]	Z	Dw [mm] [inch]	Oil [min ⁻¹]	Grease [min ⁻¹]	(L) light [N]	(M) medium [N]	(S) heavy [N]
AC bearings, sealed,	metric											
SV725A-2VZ C TA	5.00 .1969	16.00 .6299	5.00 .1969	647	1305	12	1.984 .0781	194000**	155000	7	20	40
HYSV725A-2VZ C TA	5.00 .1969	16.00 .6299	5.00 .1969	453	1305	12	1.984 .0781	290000**	194000	7	20	40
SV725A-2VZ E TA	5.00 .1969	16.00 .6299	5.00 .1969	607	1248	12	1.984	165000**	132000	7	20	40
SV788B-2VZ C TA	8.00	16.00	4.00	723	1374	13	1.984	174000**	139000	7	21	42
HYSV788B-2VZ C TA	.3150 8.00	.6299 16.00	.1575 4.00	506	1374	13	.0781 1.984	261000**	174000	7	21	42
SV708B-2VZ C TA	.3150 8.00	.6299 22.00	.1575 7.00	1298	2625	10	.0781 3.175	144000**	115000	13	40	80
HYSV708B-2VZ C TA	.3150 8.00	.8661 22.00	.2756 7.00	909	2625	10	.1250 3.175	216000**	144000	13	40	80
SV708B-2VZ E TA	.3150 8.00	.8661 22.00	.2756 7.00	1218	2510	10	.1250 3.175	122000**	98000	13	40	80
HYSV708B-2VZ E TA	.3150 8.00	.8661 22.00	.2756 7.00	853	2510	10	.1250 3.175	183000**	122000	13	40	80
SV709A-2VZ C TA	.3150 9.00	.8661 24.00	.2756 7.00	1493	2822	11	.1250 3.175	128000**	102000	14	40	80
	.3543	.9449	.2756				.1250					
HYSV709A-2VZ C TA	9.00 .3543	24.00 .9449	7.00 .2756	1045	2822	11	3.175 .1250	191000**	128000	14	43	80
SV7800A-2VZ C TA	10.00 .3937	19.00 .7480	5.00 .1969	876	1487	15	1.984 .0781	143000**	114000	8	23	40
HYSV7800A-2VZ C TA	10.00 .3937	19.00 .7480	5.00 .1969	613	1487	15	1.984 .0781	215000**	143000	8	23	40
SV7900B-2VZ C TA	10.00 .3937	22.00 .8661	6.00 .2362	1173	2047	13	2.500 .0984	128000**	102000	11	33	6
HYSV7900B-2VZ C TA	10.00 .3937	22.00 .8661	6.00 .2362	821	2047	13	2.500 .0984	192000**	128000	11	33	6
SV7000A-2VZ C TA	10.00 .3937	26.00 1.0236	8.00 .3150	2030	3879	10	3.969 .1563	115000**	92000	20	60	120
SV7000A-2VZ E TA	10.00 .3937	26.00	8.00	1905	3710	10	3.969	98000**	78000	20	60	120
HYSV7000A-2VZ E TA	10.00	1.0236 26.00	.3150 8.00	1334	3710	10	.1563 3.969	147000**	98000	20	60	120
SV7901A-2VZ C TA	.3937 12.00	1.0236 24.00	.3150 6.00	1478	2329	16	.1563 2.500	115000**	92000	12	35	7
HYSV7901A-2VZ C TA	.4724 12.00	.9449 24.00	.2362 6.00	1035	2329	16	.0984 2.500	173000**	115000	12	35	7
SV7901A-2VZ E TA	.4724 12.00	.9449 24.00	.2362 6.00	1387	2227	16	.0984 2.500	98000**	79000	12	35	7
HYSV7901A-2VZ E TA	.4724 12.00	.9449 24.00	.2362 6.00	971	2227	16	.0984 2.500	147000**	98000	12	35	7
SV7001B-2VZ C TA	.4724 12.00	.9449 28.00	.2362 8.00	2328	3603	16	.0984 3.175	101000**	80000	18	55	11
HYSV7001B-2VZ C TA	.4724 12.00	1.1024 28.00	.3150 8.00	1141	3603	16	.1250 3.175	151000**	101000	18	55	11
SV7001B-2VZ E TA	.4724 12.00 .4724	1.1024 28.00 1.1024	.3150 8.00 .3150	2184	3446	16	.1250 3.175 .1250	85000**	68000	18	55	11

GRW designation	7010	Main dimensions in [mm] [inch]			ratings DIN ISO	Ball set		Limiting :	speeds*	Preload		
Basic symbols	d	D	В	C _{or} [N]	C _r [N]	Z	Dw [mm] [inch]	Oil [min ⁻¹]	Grease [min ⁻¹]	(L) light [N]	(M) medium [N]	(S) heavy [N]
C bearings, sealed, r	netric											
HYSV7001B-2VZ E TA	12.00	28.00	8.00	1070	3446	16	3.175	128000**	85000	18	55	111
	.4724	1.1024	.3150				.1250					
SV7201B-2VZ E TA	12.00	32.00	10.00	3034	5373	11	4.763	80000**	64000	29	86	173
	.4724	1.2598	.3937	1.407	5070	1 1	.1875	100000**	00000	00	0.(170
HYSV7201B-2VZ E TA	12.00 .4724	32.00 1.2598	10.00 .3937	1487	5373	11	4.763 .1875	120000**	80000	29	86	173
SV7902A-2VZ C TA	.4/24 15.00	28.00	.393/ 7.00	2359	3586	16	3.175	95000**	76000	18	55	110
SV790ZA-ZVZ C TA	.5906	1.1024	.2756	2339	3000	10	.1250	93000	70000	10	55	
HYSV7902A-2VZ C TA	15.00	28.00	7.00	1651	3586	16	3.175	143000**	95000	18	55	110
113V7 702A 2V2 C IA	.5906	1.1024	.2756	1051	5500	10	.1250	143000	73000	10	55	
SV7902A-2VZ E TA	15.00	28.00	7.00	2213	3430	16	3.175	81000**	65000	18	55	110
	.5906	1.1024	.2756	2210	0.000	10	.1250	01000	00000	10	00	
HYSV7902A-2VZ E TA	15.00	28.00	7.00	1549	3430	16	3.175	121000**	81000	18	55	11(
	.5906	1.1024	.2756				.1250					
SV7002A-2VZ C TA	15.00	32.00	9.00	3337	5125	15	3.969	87000**	70000	26	79	15
	.5906	1.2598	.3543				.1563					
HYSV7002A-2VZ C TA	15.00	32.00	9.00	2336	5125	15	3.969	131000**	87000	26	79	15
	.5906	1.2598	.3543				.1563					
SV7002A-2VZ E TA	15.00	32.00	9.00	3131	4902	15	3.969	74000**	59000	26	79	15
	.5906	1.2598	.3543				.1563					
HYSV7002A-2VZ E TA	15.00	32.00	9.00	2192	4902	15	3.969	111000**	74000	26	79	158
	.5906	1.2598	.3543				.1563					
SV7903A-2VZ C TA	17.00	30.00	7.00	2402	3554	16	3.175	88000**	70000	18	55	11
	.6693	1.1811	.2756	1 (0 0	0.5.5.4		.1250					
HYSV7903A-2VZ C TA	17.00	30.00	7.00	1682	3554	16	3.175	132000**	88000	18	55	11
SV7903A-2VZ E TA	.6693 17.00	1.1811 30.00	.2756 7.00	2254	3399	16	.1250 3.175	75000**	60000	18	55	1.1.
3V79U3A-ZVZ E TA	.6693	1.1811	.2756	2234	2244	10	.1250	/3000	80000	10	55	110
HYSV7903A-2VZ E TA	17.00	30.00	7.00	1578	3399	16	3.175	112000**	75000	18	55	11
1113V7903A-2V2 L IA	.6693	1.1811	.2756	1370	5544	10	.1250	112000	7 3000	10	55	11
SV7003-2VZ C TA	17.00	35.00	10.00	4415	6654	14	4.763	65000**	54000	34	102	20
017 000 212 0 171	.6693	1.3780	.3937				.1875		01000		.02	201
HYSV7003-2VZ C TA	17.00	35.00	10.00	3091	6654	14	4.763	96000**	69000	34	102	20.
	.6693	1.3780	.3937				.1875					
SV7003-2VZ E TA	17.00	35.00	10.00	4143	6363	14	4.763	56000**	46000	34	102	20
	.6693	1.3780	.3937				.1875	N. St.	AAX	JA	$\Delta \omega$	VV.
HYSV7003-2VZ E TA	17.00	35.00	10.00	2900	6363	14	4.763	82000**	59000	34	102	20.
	.6693	1.3780	.3937				.1875					
SV7904A-2VZ C TA	20.00	37.00	9.00	3868	5394	16	3.969	70000	56000	27	81	16
	.7874	1.4567	.3543		A		.1563	100 th	TAN			
HYSV7904A-2VZ C TA	20.00	37.00	9.00	2708	5394	16	3.969	105000	70000	27	81	162
	.7874	1.4567	.3543				.1563		7			
SV7005A-2VZ C TA	25.00	47.00	12.00	7909	10661	17	5.556	56000	44000	53	160	320
	.9843	1.8504	.4724	5504	10//1	17	.2187		E / 000		1.4.0	
HYSV7005A-2VZ C TA	25.00 .9843	47.00 1.8504	12.00 .4724	5536	10661	17	5.556 .2187	83000	56000	53	160	320

* The indicated speed limits are guidelines for spring-loaded single bearings with low loads; depending on the respective application, higher or lower speed limits may apply in application.

• Subject to change. Additional types on request!



** For use with oil lubrication, these bearings are also available without shields.
Almost all bearing types can also be enhanced with GRW XTRA. Detailed information you can find on page 79 and following.



Profiled rollers

Profiled rollers are double-row ball bearings; which means they are able to accept axial loads in both directions, as well as high radial loads. Usually, the contact surface is shaped like a Gothic arch; the contact surface and shaft touch each other in two locations.

On request, other contour surface designs are available (e.g. V groove, spherical outer ring, etc.).

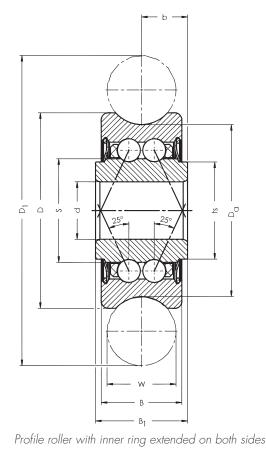
Inner and outer rings can be made of chrome steel 100Cr6 or corrosion-resistant chrome steels X65Cr13 or X30CrMoN 15-1. Balls can be made of chrome steel 100Cr6, X65Cr13 or ceramic.

GRW profiled rollers have non-contact shields. On request, contact seals (e.g. Teflon[®], NBR) are available as an alternative. The rollers are lubricated for life and are also available with FDA-approved and/or autoclavable lubricants.

For further information please contact your nearest GRW Sales Representative.

Basic symbol	Drawing no.	d	D _a	D	D	w	В	B ₁	b	S
687/603282-2RZ	604623	5	_	17	27	6	7	8	4	9
687/603282-2Z	603282	5	_	17	27	6	7	8	4	9
687/602057-2Z	602057	5	-	17	25	5	7	8.5	5	9
687/601938-2Z	601938	5	_	17	27	6	7	8.5	5	9
687/601935-2Z	602055	5	-	16	22	4	7	8.5	5	9
687/601935-2Z	601935	5	-	16	22	4	7	8.5	5	9
608/602030-2ZF	604976	8	-	24	34	6	11	11	5.5	11.8
608/602030-2ZF	602030	8	-	24	34	6	11	11	5.5	11.8
608/602024-2ZF	602024	8	-	24	37	8	11	12.5	7	11.8
608/601947-2ZF	602053	8	-	24	34	6	11	12.5	7	11.8
608/601947-2ZF	601947	8	-	24	34	6	11	12.5	7	11.8
6201/604947-2Z	604947	12	-	35	51.3	10	15.9	15.9	7.95	18.28

Subject to change.



Bearing units

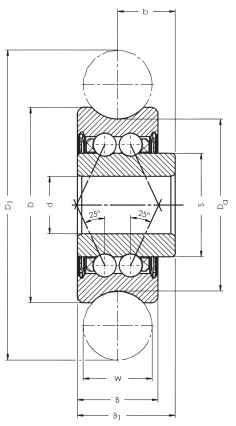
Bearing units are pre-mounted assemblies, comprising of at least one ball bearing, shaft or housing, optional spacers, shims or spring washers.

GRW assembles the stacked components in bearing units primarily by using adhesives. Backlash free bearing units are produced cost effectively by precisely gluing the bearings under an axial pre-load. GRW has engineered special gluing equipment and techniques to ensure high accuracy and strength.

When using GRW bearing units, customers will profit from the following benefits:

- Cost advantages by eliminating possibility of improper customer assembly.
- Pre-mounted units are easier to handle than single bearings.
- At GRW the bearings are mounted in a clean room under optimum conditions.





Profile roller with inner ring extended on one side

- Depending on the application requirements, other functional elements may be integrated in the bearing units, for example springs and seals.



Thin-section bearings

Thin-section bearings are bearings with very thin ring cross-sections (light ISO dimension series 67/68) or bearings with identical cross-sections, independent of their bore diameter (inch series: Extra Thin Series, Thin Series).

In addition to their small footprint and low weight, they are characterized by low torque and high rigidity.

Thin-section bearings are available in the following versions: open (standard), with closures, with an extended inner ring, with a flanged outer ring and as an angular contact or full-complement bearing at a maximum outside diameter of 40 mm.

The closures are available in -27 and -2TS versions

By default, thin-section bearings are all ABEC5. Please inquire about other available versions (e.g. Superduplex) ABEC7, and ABEC9.

Basic symbol	c	I	D	•	1	В	r,	min	d	min	d	max	Da	max
Busic symbol	[mm]	[inch]	[mm]	[inch]	[mm]	[inch]	[mm]	[inch]	[mm]	[inch]	[mm]	[inch]	[mm]	[inch]
15875A	15.875	.625	22.225	.875	3.967	.156	0.25	.010	16.9	.665	17.9	.705	20.6	.811
15875A-2Z	15.875	.625	22.225	.875	4.978	.196	0.25	.010	16.9	.665	17.9	.705	20.6	.811
15875A-2TS	15.875	.625	22.225	.875	4.978	.196	0.25	.010	16.9	.665	17.2	.677	20.6	.811
19050A	19.050	.750	25.400	1.000	3.967	.156	0.25	.010	20.1	.791	21.1	.831	23.7	.933
19050A-2Z	19.050	.750	25.400	1.000	4.978	.196	0.25	.010	20.1	.791	21.1	.831	23.7	.933
19050A-2Z	19.050	.750	25.400	1.000	4.978	.196	0.25	.010	20.1	.791	20.4	.803	23.7	.933
22225A	22.225	.875	28.575	1.125	3.967	.156	0.25	.010	23.3	.917	24.3	.957	26.9	1.059
22225A-2Z	22.225	.875	28.575	1.125	4.978	.196	0.25	.010	23.3	.917	24.3	.957	26.9	1.059
22225A-2TS	22.225	.875	28.575	1.125	4.978	.196	0.25	.010	23.3	.917	23.6	.929	26.9	1.059
26988A	26.988	1.063	33.338	1.313	3.967	.156	0.25	.010	28.1	1.106	29.1	1.146	31.7	1.248
26988A-2Z	26.988	1.063	33.338	1.313	4.978	.196	0.25	.010	28.1	1.106	29.1	1.146	31.7	1.248
26988-2TS	26.988	1.063	33.338	1.313	4.978	.196	0.25	.010	28.1	1.106	28.4	1.118	31.7	1.248
31750A	31.750	1.250	38.100	1.500	3.967	.156	0.25	.010	32.8	1.291	33.8	1.331	36.4	1.433
31750A-2Z	31.750	1.250	38.100	1.500	4.978	.196	0.25	.010	32.8	1.291	33.8	1.331	36.4	1.433
31750A-2TS	31.750	1.250	38.100	1.500	4.978	.196	0.25	.010	32.8	1.291	33.1	1.303	36.4	1.433
34925A	34.925	1.375	41.275	1.625	3.967	.156	0.25	.010	36.0	1.417	37.0	1.457	39.5	1.555
34925A-2Z	34.925	1.375	41.275	1.625	4.978	.196	0.25	.010	36.0	1.417	37.0	1.457	39.5	1.555
34925A-2TS	34.925	1.375	41.275	1.625	4.978	.196	0.25	.010	36.0	1.417	36.3	1.429	39.5	1.555

Subject to change.

Hybrid and full ceramic ball bearings

Conventional ball bearings are limited when operating at high temperatures, in a vacuum, or in a corrosive environment. All ceramic bearings have proven to be ideally suited for these extreme applications.

Zirconium oxide (ZrO₂) and silicon nitride (Si₃N₄) are typical materials used in all ceramic bearings. Both provide excellent corrosion and temperature resistance as well as other mechanical properties.

Material properties:

Properties	Unit	Si ₃ N ₄ HY	ZrO ₂ ZO
Density	g/cm³	3.2	6.05
Hardness	Rc	> 75	> 69
E-module	GPa	320	200
Poisson coefficient		0.26	0.2
Linear expansion coefficient	x10-6 K-1	2.9	10
Max. temperature	°C	800	600
Corrosion resistance		very good	good
Electrical conductivity		insulator	insulator





High chemical resistance

All ceramic ball bearings have specific advantages for applications with mixed-torque because they remain operative for a longer period of time than conventional steel bearings even in the case of lube deprivation.

Corrosion resistance

All ceramic bearings resist cold micro welding to other materials which allows for particularly low adhesive wear. Certain applications make use of conventional bearings almost impossible. For example: corrosive material resistance of all ceramic bearings allows for usage in chemical applications.

Thermal expansion

Full ceramic bearings will remain dimensionally stable even at high temperature fluctuations.

Non-magnetic and current insulation

The non-magnetic properties of ceramic materials prevent interference with magnetic fields and furthermore acts as an insulator preventing current flow.



Special ball bearings

GRW develops and produces a complete range of custom bearing options.

Superduplex bearings

Superduplex bearings are also known as double row deepgroove ball bearings or angular contact ball bearings featuring split inner or outer rings. One of the ring sets, either outer or inner, consist of a double row integral set of raceways.

This compact design permits easy handling and assembly. The inner or outer split rings are paired according to customer specifications ensuring that GRW bearings will meet the required axial preload.



Extraduplex bearings are double-row deep groove radial bearings or angular contact ball bearings with a split inner or outer ring. One floating ring is accurately preloaded and then laser-welded in place. This style of bearing prevents radial offset or changes in axial preload during assembly.





Tandemduplex bearings

Tandemduplex bearings are designed with double-row deepgroove bearings. The raceways are extremely close to each other (in the micron range). These bearings are designed to handle both radial loads and axial loads in one direction by ensuring that the load is evenly distributed to all balls.

Bearings with custom outer geometries

GRW can produce single or double-row bearings with a spherical faced or grooved outer ring and also can provide molded and plastic rubber type assemblies.





Integrated shaft bearings

Bearing and shaft can be combined to provide an integrated assembly. In this design the raceway is ground on the shaft and the bearing assembly is delivered completely assembled ready to use.

Bearing / housing assemblies

For these special designs, the raceway of the outer ring is ground directly into the housing. Complex housings, flanges and threaded mounting holes maintain the tight tolerances necessary for proper installation.

Precision components

GRW manufactures precision spacers and precision components that incorporate threads, steps, grooves, bores, etc. to tolerances in the micron (μ) range.



























Coated bearings

Sometimes the use of conventional lubricants is impossible especially in applications where there is exposure to extremely high or low temperatures, ultra-high vacuum, or in close proximity to optical systems.

The solution in these cases may be special coatings with gold, silver, MoS_2 , or Teflon[®]. These thin layers act as a dry film lubricant. Development of this technology has made applications possible even at temperatures of -270 °C to +400 °C or in a high vacuum.

Protection against wear is also an advantage of using thin coated bearings. Raceways, balls, or outer surfaces can be thinly coated to meet each application's requirements. Possible uses for these types of coatings are profiled rollers, paper cutting blade wheels, bearings used in chemical or food processing industry, medical instruments, aerospace and vacuum technology.

As each coating can be applied by a variety of technologies, GRW will work with each customer to select the optimum coating process to meet your application requirements.

Special developed for applications in extreme conditions we offer our customers special ball bearing solutions with the new coating system XTRAcoat. Further information you can find on the following pages.





XTRAcoat / The new GRW coating system **XTRAlube / Lubrication for longer life XTRAIon** / The Premium retainer material



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XTRA 。



XTRA Enhancing Performance!

In order to successfully meet the challenges of the market, our products are being continuously developed and their performance improved, based on the latest innovations from GRW.

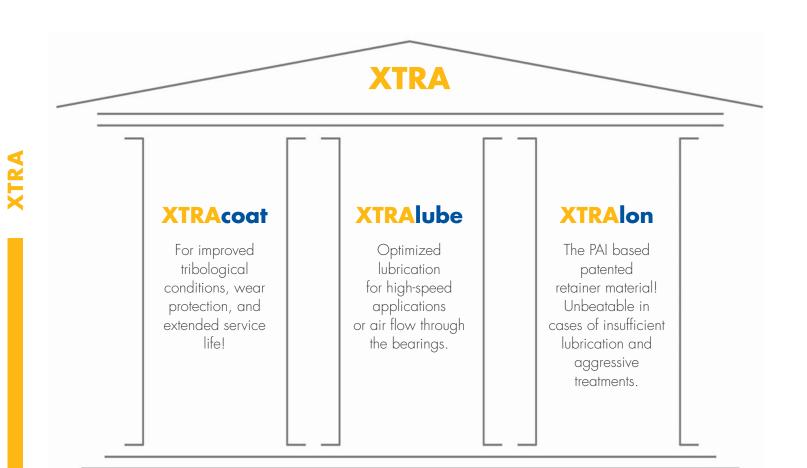
Developments that we have achieved in the areas of product design, ball bearing steels, retainer design and materials, lubricants and surface coatings are the basis for the technological leadership the company has today.

With GRW XTRA, we are not so much reinventing the ball bearing but using our expertise to improve performance levels in terms of running noise, service lifetime and speed for instance. The ball bearing designed by GRW to your individual requirements acquires superior performance due to XTRA.

XTRA – the GRW solution for your challenges!

For more information about XTRA contact our sales engineers. They will be glad to advise you.

🖀 worldwide: +49 (0) 93 65/819 - 440 🖀 USA: +1 (804) 328 0900 ⊠ xtra@grw.de



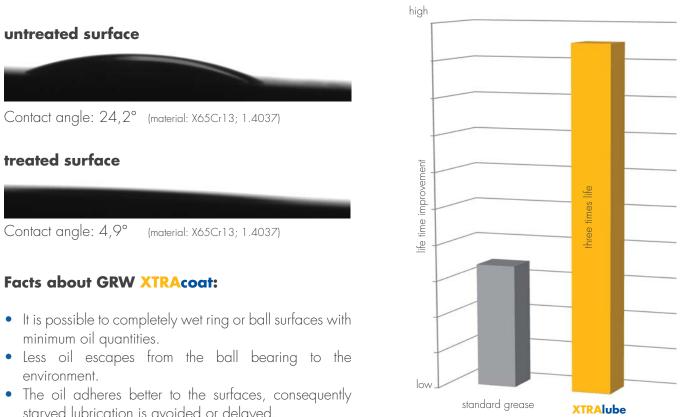
XTRAcoat

Originally developed for extreme conditions in handpiec-For the toughest operating cones of medical and dental equipment and however excelditions in special applications, lently suitable for any other application, we offer our cus-GRW relies on developing its tomers special ball bearings with the new coating system own lubricants, which have the potential for significantly XTRAcoat. longer life: XTRAlube.

The coating developed exclusively for GRW equips the ball bearing components with the special capability to The new **XTRAIube** developed in the GRW laboratory bind the applied grease to surfaces, and therefore delivers outstanding results both in the test criteria which to prevent as far as possible an insufficient lubrication GRW considers crucial and in the various functional tests. It also has the special ability to adhere to the contact sursituation from occurring, even under adverse operating conditions. faces of the inner ring and outer ring much better than standard greases.

Which leads to a significantly higher service life, even in extreme cases where hygienic cleaning is done and maintenance is omitted.

Validating the effect of XTRAcoat at a contact angle measurement with dental maintenance oil, can be clearly seen that the contact angle falls below 5° using **XTRAcoat**



- starved lubrication is avoided or delayed.
- Bearing life is prolonged.



XTRAlube



In the specific case of ball bearings for dental turbines this property is particularly sought after, because the air extracted from the turbine flows partly through the ball bearings and transports the grease reservoir to the outside very rapidly. This leads to a situation of inadequate lubrication, which is responsible for the failure of the ball bearings.

Average value at life test on the GRW test bench Orakel III. Initially lubricated and no relube during test.

XTRA

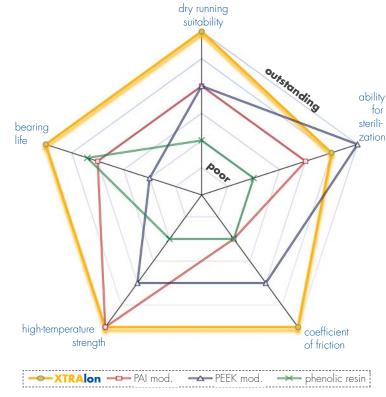


XTRAlon

Our premium material is designed for the most demanding requirements in terms of friction, thermal stability and wear. The unique production method involving the chemical binding of solid lubricant to the base polymer polyamidimide (PAI) creates a homogeneous, dense fabric, which offers little opportunity for attack by the superheated steam during autoclaving.

The fine distribution of solid lubricant and the chemical bond to the base material means that the exceptional property of dry-running suitability is obtained, even in extreme applications where idle speed of $n \times dm > 1.000.000$ mm/min are the norm. In internal tests on GRW's own test rigs, service lifetimes of up to 15 hours were attained with completely dry ball bearings. All conventional retainer materials fail after only a few minutes in the same test.

The SEM images show the surfaces of XTRAIon and PAI mod. after 1.000 cycles of sterilization by steam under pressure. It can be clearly seen that the surface structure of **XTRAIon** is preserved, while the PAI mod. has a very jagged surface.



Performance overview of standard retainer materials compared to GRW XTRAIon used in high-speed dental handpieces.



As part of a development project for a major GRV customer, extremely high performance improvement over the current product design were obtained, conjunction with XTRA developments. As part of this parameters such as running noise, product service life and idle speed were tested on GRW internal test rigs an optimized by applying XTRA advancements.

GRW customers benefit from our XTRA bearings

- Silent bearings ensure a more pleasant work in the dental field and any other application
- The high product reliability of GRW XTRA bearings ensures longer life time and reduces costs.
- Higher idle speed.

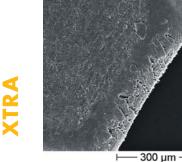
life time

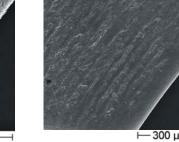
retainer friction

operating noise

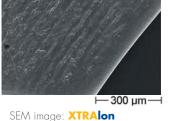
low

• GRW XTRA makes ball bearings resistant and more durable despite poor care, extreme temperatures and highest speeds.











Life time test with XTRAIon modified ball bearings without initial lubrication:



Effect of the retainer material to the life time of dental turbines without any initial lubrication tested on Orakel III test bench (n=350.000 min⁻¹).

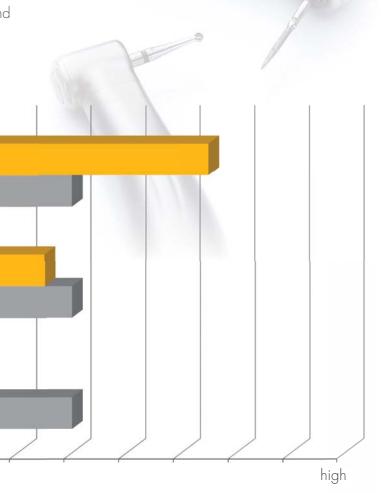
Effect of retainer design on the running properties of high-speed dental ball bearings.



Measurable target	2013	2014 XTRA	Improvement
Noise [dB(A)]	70	65	- 29% *
Life time [h]	90	260	+ 189%
Early failure [h]	> 50	> 120	+ 140%
Idle speed [rpm]	360.000	370.000	+ 3%

Improvement of a high speed handpiece of a GRW customer.

* Decrease by 10 dB is a reduction of the noise level by 50% (logarithmic scale).



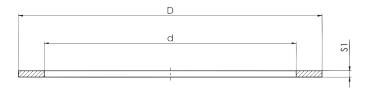
GRW XTRA retainer design

ordinary retainer design

CT R



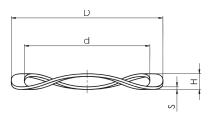
Accessories



Shims AS

For production engineering purposes, shims are often used to balance the accumulation of tolerances (tolerance chains) and axial tolerances.

GRW spring washers are made of corrosion-proof 1.4310 (AISI 301) spring wire. They are heat-treated, burr-free, and have an extremely fine surface finish



Spring washers WF

Spring washers are used for defined axial preloading of bearings, particularly for miniature and small ball bearings. The manufacture of these spring washers includes cutting and punching processes. Through a subsequent finishing process, they can be calibrated to provide highly accurate preload tolerances for special applications.

GRW spring washers are made of corrosion-proof 1.4310 (AISI 301) spring wire. They are heat-treated, burr-free, and have an extremely fine surface finish. Our spring washers are designed with 3 waves ensuring even support of the bearing during axial preloading.

	I	Dimensions [mm]						
Shims		Spring washers		Compatible sizes				
d x D	s	(d x D x H x s)	Spring constant [N/mm]	on shafts	in housings			
AS 1.55 x 2.50	0.15	_	_	68/1,5, 69/1,5	_			
_	-	WF 1.60 x 2.90 x 0.40 x 0.06	50.0	_	_			
-	- 0.10	WF 1.90 x 2.80 x 0.50 x 0.08	60.0	-	-			
AS 2.00 × 4.30	0.16 0.20	-	_	-	-			
AS 2.25 × 3.20	0.08 0.10	WF 2.15 x 3.10 x 0.50 x 0.08	54.9	682, 692, 5/64	-			
AS 2.80 × 3.90	0.08 0.10	WF 2.70 x 3.80 x 0.50 x 0.08	52.0	60/2,5,68/2,5,69/2,5,3/32	68/1,5,691,1191			
AS 3.05 x 4.50	0.10 0.16 0.20	-	-	-	-			
AS 3.30 × 4.40	0.08 0.10 0.12	WF 3.20 x 4.30 x 0.50 x 0.10	32.5	623, 683, 693, 1/8A, 1/8B, 3175,1/8A/6, 1/8B/083	_			
AS 3.50 x 5.00	0.08	_	—	-	_			
AS 3.80 x 4.90	0.08 0.10 0.12	WF 3.70 x 4.80 x 0.55 x 0.10	32.0	_	682,69/1,5			
AS 4.05 × 5.50	0.10 0.20	_	_	-	_			
AS 4.30 x 5.85	0.10 0.12 0.15	WF 4.20 x 5.75 x 0.65 x 0.12	40.0	604, 624, 634, 684, 694, 3967	68/2,5,692			
AS 4.90 x 6.20	0.10 0.12 0.15	WF 4.80 x 6.10 x 0.60 x 0.12	37.0	3/16, 4763A, 4763B	5/64, 3175			
AS 5.20 x 6.75	0.15	_	_	-	—			
AS 5.30 x 6.85	0.10 0.12 0.15	WF 5.20 x 6.75 x 0.65 x 0.12	22.0	625, 635, 685, 695	683, 69/2,5			
AS 5.50 x 8.50	0.40	_	_	-	-			
AS 6.30 x 7.85	0.12 0.15 0.18	WF 6.20 x 7.75 x 0.70 x 0.15	38.0	626, 686, 696	60/2,5,693,3/32, 1/8A,3967,4763A			
AS 6.70 x 9.40	0.10	_	-	- / //	<u>Andre</u> ha inte			
AS 7.30 x 8.80	0.12 0.15 0.18	WF 7.20 x 8.70 x 0.90 x 0.15	28.5	607, 627, 687, 697	684			
_	-	WF 7.20 x 12.00 x 1.55 x 0.13	41.8	607, 627	6350B, 7938, 1/8B/083			
AS 8.30 × 9.80	0.10 0.15 0.18	WF 8.20 x 9.70 x 0.85 x 0.18	26.0	608, 688, 698, 7938	623			
AS 9.30 x 10.80	0.20	WF 9.20 x 10.70 x 1.15 x 0.18	22.0	609, 629, 689, 699	685, 694			
AS 10.30 x 11.80	0.20 0.18 0.20 0.22	WF 10.20 x 11.70 x 1.05 x 0.20	18.5	6000, 6800, 6900,3/8	604			
_	-	WF 10.50 x 15.80 x 1.85 x 0.25	77.0	6000	625, 634			
AS 11.30 x 12.80	0.18 0.20 0.22	WF 11.20 x 12.70 x 1.30 x 0.20	16.0	- 48	624, 686, 695			
AS 12.30 x 13.80	0.20 0.22 0.22 0.25	WF 12.20 x 13.70 x 1.30 x 0.22	20.0	-//83	687			
AS 13.30 x 14.80	0.20 0.22 0.25	WF 13.20 × 14.70 × 1.30 × 0.22	13.0		696			
AS 14.35 x 15.80	0.22 0.25 0.30	WF 14.20 x 15.65 x 1.55 x 0.25	17.0	ALL AND	625, 634, 688, 1/4A			
AS 15.35 x 16.80	0.22 0.25 0.30	WF 15.20 × 16.65 × 1.55 × 0.25	14.5	CEER \	689, 697			
AS 16.00 x 22.00	0.10	WF 15.80 x 21.80 x 1.60 x 0.20	10.0	(VII)	3/8			
AS 16.40 x 18.80	0.25 0.30 0.35	WF 16.20 x 18.55 x 2.15 x 0.30	28.5		607, 626, 635, 6800, 698, 1/4			
Naterial 1,4310 (AISI 301)		lanning to use shims and spring washers please of	hock on availe	ability Other sizes on request. Subject to d	ango Minimum quantity 100 pieces			

Material 1.4310 (AISI 301). Before planning to use shims and spring washers, please check on availability. Other sizes on request. Subject to change. Minimum quantity 100 pieces.



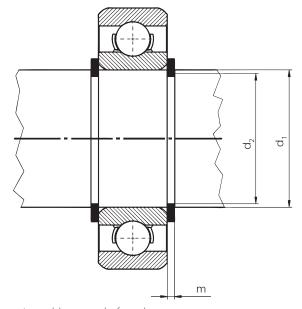


Accessories

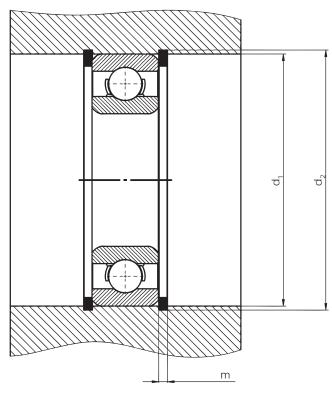
Retaining rings – (shaft circlips WSR, bore retaining rings BSR)

Retaining rings are precision engineered components designed to be applied on shafts or in bores providing a shoulder that accurately positions, locates and retains parts of an assembly. They are especially useful with small and evenly distributed axial and radial loads. It is important to ensure that the face of the retaining ring does not touch the edge radius of the bearing. If the face does touch the radial edge, we recommend that you use our shims in conjunction with our retaining rings.

GRW retaining rings are constructed from colddrawn spring wire 1.4310 (AISI 301), which exhibits a constant cross section. They are corrosion-proof and free of any scale or burrs.



Assembly using shaft circlips



Assembly using bore circlips

Shaft circlips

Bore circlips

Туре	Dimensions [mm]										
	Shaft		Split lock	Gro							
	dı	d ₃ max.	b ± 0.10	s ± 0.02	d ₂ - 0.05	m + 0.03					
VVSR 3	3	2.60	0.50	0.30	2.70	0.33					
WSR 4	4	3.60	0.50	0.30	3.70	0.33					
WSR 5	5	4.50	0.70	0.40	4.60	0.44					
WSR 6	6	5.45	0.70	0.40	5.60	0.44					
WSR 7	7	6.45	0.70	0.40	6.60	0.44					
WSR 8	8	7.35	0.90	0.50	7.50	0.55					
WSR 9	9	8.30	0.90	0.50	8.50	0.55					
WSR 10	10	9.25	0.90	0.50	9.50	0.55					

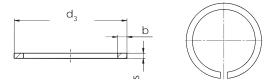
Material 1.4310 (AISI 301). Subject to change. 1000 pieces per pack.

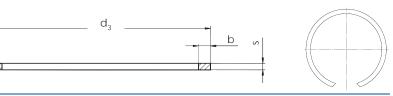
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Туре	Shaft		Gro			
	d,	d ₃ min.	Split lock b ± 0.10	S ± 0.02	d ₂ - 0.05	m + 0.03
BSR 4	4	4.40	0.50	0.30	4.30	0.33
BSR 5	5	5.45	0.50	0.30	5.30	0.33
BSR 6	6	6.45	0.50	0.30	6.30	0.33
BSR 7	7	7.50	0.50	0.30	7.30	0.33
BSR 8	8	8.60	0.70	0.40	8.40	0.44
BSR 9	9	9.60	0.70	0.40	9.40	0.44
BSR 10	10	10.65	0.70	0.40	10.40	0.44
BSR 11	11	11.65	0.70	0.40	11.40	0.44
BSR 12	12	12.75	0.90	0.50	12.50	0.55
BSR 13	13	13.75	0.90	0.50	13.50	0.55
BSR 14	14	14.80	0.90	0.50	14.50	0.55
BSR 15	15	15.80	0.90	0.50	15.50	0.55
BSR 16	16	16.85	0.90	0.50	16.50	0.55
BSR 1 <i>7</i>	17	17.85	0.90	0.50	17.50	0.55
BSR 19	19	20.00	1.10	0.60	19.60	0.66

Material 1.4310 (AISI 301). Subject to change. 1000 pieces per pack.









Test engineering

Orakel III

The test module developed by GRW can be freely lined to form test series. Automated and with a minimum of personnel expenditure, it tests the lifetime of high-speed dental handpieces, allowing for fast and efficient comparison of a development stage with the previously determined reference.

For evaluation of the performance characteristics of the entire system, the test process in respect of the mechanical load cycle and test criteria can be parameterized and is thus objectively reproducible. Calibration, test parameter settings and documentation of results are carried out on a commercially available PC. The actual test is carried out self-sufficiently.

Benefits:

- Up to 7,000 cycles can be executed without interruption.
- Uniform test process can be exactly reproduced.
- The operation of the modules only requires power and clean compressed air.
- Testing capacities can be expanded at any time by adding additional modules.
- Easy documentation: For each cycle, the measured speed is stored and can be written in a text file along with details of the completed testing time.
- Up to 10 modules can be controlled by one PC.



Note: Orakel III, the test module developed by GRW, is available for purchase. Contact us for more details.

Speedmaster

The GRW Speedmaster is a noncontact speedmeasuring device especially designed for high RPM rotating instruments used in the dental industry.

It may also be used for other high-speed applications such as motors or high-frequency spindles.



Note: Speedmaster, the test module developed by GRW, is available for purchase. Contact us for more information.

The set includes: the basic measuring unit, AC adapter, speed sensor, permanent magnet, a hard metal test probe for clamping in the dental instrument, and a measuring stand to hold the speed sensor.

Measurement Principle

A test probe or a motor shaft is magnetized by means of the attached permanent magnet. The sensor is positioned 1 to 10 mm away from the magnetized shaft. When the shaft rotates, the weak magnetic field is recorded by the special GRW sensor, then amplified and displayed in RPM, or revolutions per minute.

The non-contact measurement is designed for speeds from 20,000 to 600,000 min-1.

This device has proven to be particularly useful in development and production as well as in the repair of dental turbines and surgical handpieces.

GRW laboratory services

GRW - the specialists in high-precision miniature ball bearings now offer laboratory services as well. Do you want to analyze materials? Do you need surface treatment but do not have your own laboratory or do you simply lack the expertise?

Then act flexibly and make use of the services of a competent analysis and chemistry laboratory!

We are the right partner, especially when it comes to such demanding procedures as FTIR spectroscopy with ATR technology or the functional and decorative gold plating of components.

GRW offers the following services:

General analysis, e.g. the determination of

- Ha •
- Acid concentration
- Oil or preservative content
- Evaporation residue
- Nitrite levels

Lubricant analysis with determination of protection by means of

- Dissolving and filtering
- Microscopy
- FTIR analysis

Surface treatments

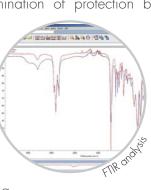
- Gold plating
- Ultrasonic cleaning
- Hot and cold bronze finishing
- Passivating high-alloy steels

Medical hygiene treatments

- Steam pressure sterilization
- Thermal desinfection

Condensation – and salt spray test

 Corrosion testing according to DIN 50021 / ASTM B117-73







As a partner of laboratory network GRW is able to offer you additional services apart from our own spectrum:

Examinations with scanning electron microscope (SEM) and X-ray spectroscopy (EDX)

X-ray fluorescence analysis (RFA)



- Detailed analysis by means of differential scanning calorimetry (DSC)
- Thermal gravimetric analysis (TGA)





Proper handling of GRW high-precision miniature bearings

GRW ball bearings are manufactured and packaged with extreme care to avoid contamination, corrosion, and other external influences on the bearings. When mounting ball bearings, please mind:

- Bearings should be stored in their original package in clean, dry rooms under constant temperature conditions.
- Bearings should only be removed from their original package shortly before they are mounted. Usage of gloves, finger cots, and tweezers are recommended.
- Assembly location has to be clean and bright. All mating parts have to be clean. A hard surface is preferred.
- When mounting a ball bearing, the assembly force must not be applied over the balls. Suitable mounting tools must be used. Non-compliance with these instructions may easily result in damage to balls or raceways, for example ball indentations may occur in the raceway.
- If glued interfaces are used, ensure that any excess glue does not enter the bearing.
- Re-lubrication should only be carried out with a lubricant of the same type and purity.

- We recommend to have the bearings lubricated by GRW as this is executed in a clean room shortly before packaging.
- Selective sorting of all mating parts will help to guarantee the proper fit of the bearing to the shaft or housing.
- We recommend a running in process for greaselubricated bearings prior to use at low speed to achieve optimum distribution of the lubricant.
- Electrical current running through the bearing should be avoided.

Bearing Analysis

Based on over 70 years of expertise, GRW can provide ball bearing analysis to establish the root cause of failure or to estimate the remaining life of the ball bearing. For more information about bearing analysis, please contact your nearest GRW Sales Representative.

Valuable results can be achieved when bearings are disassembled and examined after a certain period of operation before failure has occurred. Marking of the bearing rings during disassembly can help to reproduce original assembly characteristics.



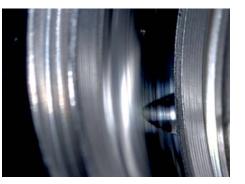




Shaft assembly

Damage due to improper handling

	Possible cause											
Defect characteristics	Contami- nation	Assembly	Assembly tools	Adhesive	Lubricant	Termpera- ture	Speed	Load	Storage	Ambient media	Fitting/ contact	Design
Noisy	Х	×		Х	×							Х
Mounting problems			х								Х	Х
Seized bearing	Х	Х		х		×	Х	Х		Х	Х	
Corrosion	Х								х	Х	х	
Coloration						х				Х		
Cracked rings								Х			Х	





Ball indentation in raceway

Lube deprivation
ct Worldwide: +49 (0

Contact USA: +1 (804) 328 0900 • www.grwbearing.com





Indentations in raceway caused by particles



Packaging

Correct packaging protects bearings from contamination, corrosion and damage during transport and storage. We recommend the package to open just prior to mounting and to use bearings with opened packages as soon as possible.

Each bearing package is labeled with the exact design specification and the respective product lot number, factory batch number, and the packaging date of the bearing.

Our Standard packaging options are as follows:

Strip Packaging "CP"

Our standard packaging contains ball bearings in one strip or pill pack, sealed individually in transparent synthetic film packets with a white backing. The guantity per strip depends upon the outside diameter of the bearing.



Bearings are bulk packaged in a transparent synthetic film pack and sealed under vacuum. The quantity per vacuum pack depends on the size of the bearing or as specified by the customer.





Spindle bearing Packaging "CP1P"

Spindle bearings are packed in a separate envelope marked 'GRW' (CP1) and boxed individually (CP1P) to avoid damaae.



Special Packaging

GRW offers a wide range of packaging options based upon our customer's requests and the requirement profile of the bearing, for example, stick packaging or aluminum envelopes.

GRW quality: internationally certified DIN EN ISO 9001

GRW is an international enterprise specializing in development and production of high-precision miniature ball bearings. Ensuring our customers complete satisfaction is our top priority. By continually improving our products and processes, we ensure the long-term success of our company.

To achieve these goals we introduced a management system that evolves with the future requirements of each market. Our corporate strategy, based on growth and innovation, is the basis for a successful partnership with our customers and suppliers.

Our integrated management system is based on DIN EN ISO 9001:2008 and is certified in four specific areas:

- 1. Organizational Manual
- 2. Key Performance Indicators (KPI)
- 3. Process Definitions and Defined Responsibilities
- 4. Process Control Documentation (work and test instructions) including supporting documents (e.g. quality check lists, forms)



The Organizational Manual includes a Management section addressing our customers, employees and suppliers. It contains our corporate principles and corporate policy. Special sections contain job descriptions and Key Performance Indicators. These critical areas of measurement contain the controlling documentation for organizational process and product quality as well as continuous improvement.







Manufacturing in a Nut Shell

GRW high-precision ball bearings are used in a variety of industries and applications.

Before they leave our factory, they have passed several complex manufacturing steps.

Their journey starts in the turning department where our highprecision turning machines produce bearing rings from a variety of steels used by GRW.



Turning department





Measurement room

Honing is the last step before assembly. The finished, bearing rings run through a final process on machines co-developed by GRW for surface finishing of the raceways.

During the final assembly, finished components are sorted and selected to guarantee customer satisfaction and in some cases automated assembly can be used to assemble, lubricate and package bearings.





After heat treat, all critical dimensions and raceway geometries are precisely machined to the micron (µ). Interim quality measurements are made in the measurement room



Grinding department





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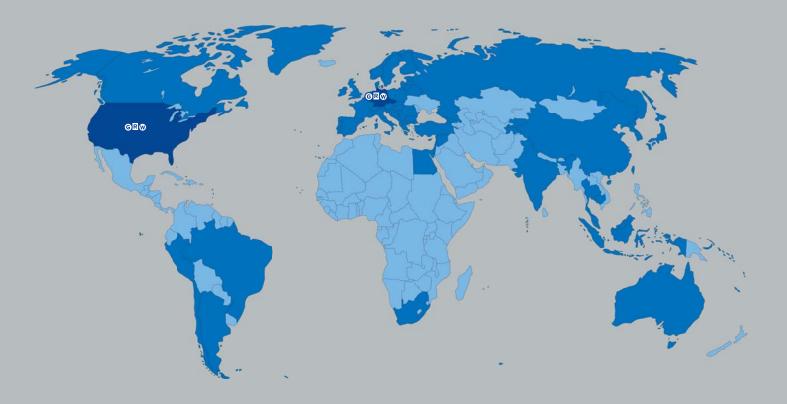
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